

Biobehavioral Health Building

The Pennsylvania State University

Daniel Bodde

Structural Option

Advisor – Heather Sustersic



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Building Introduction

Location:

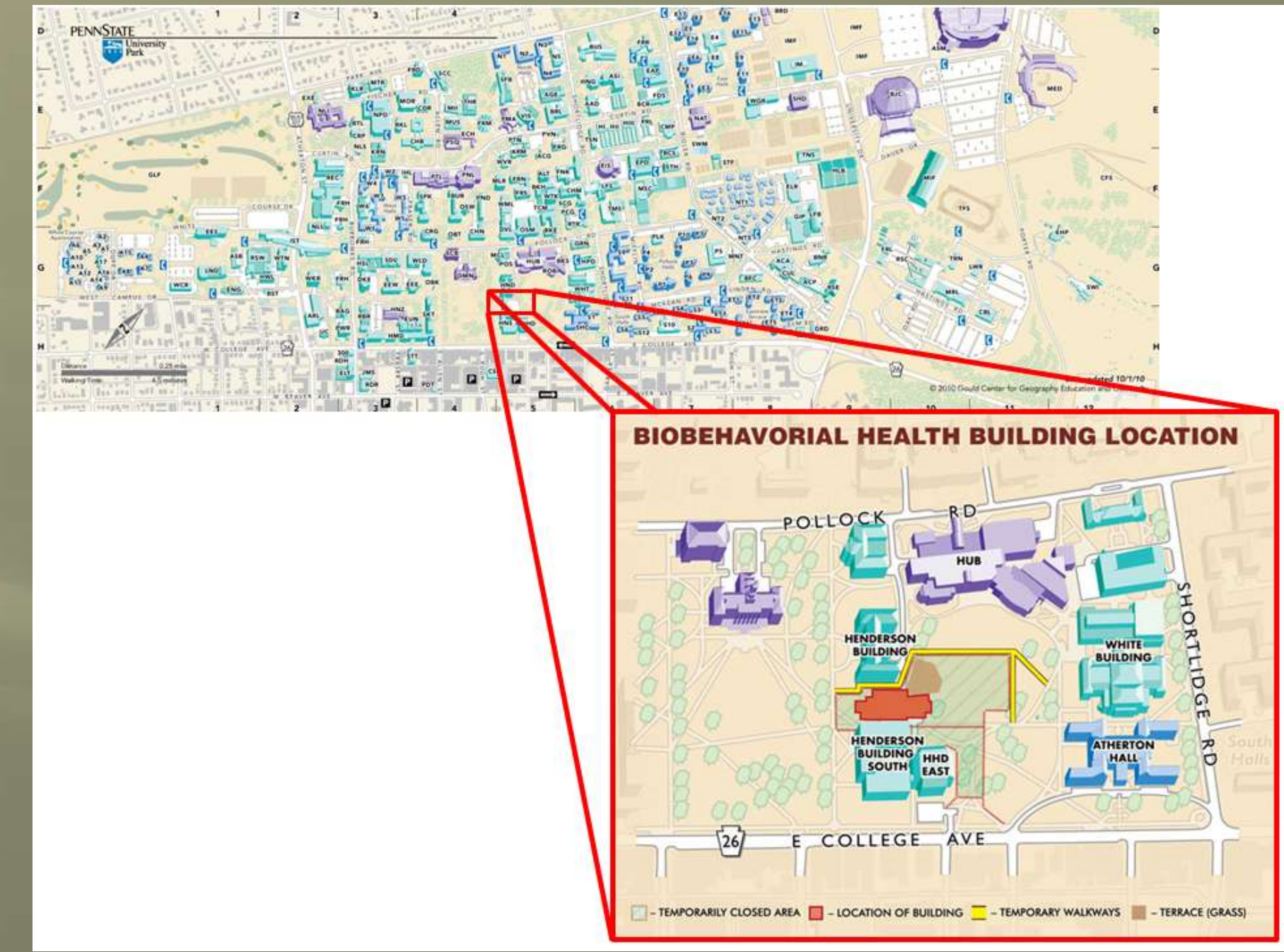
- The Pennsylvania State University
University Park, PA

Project Size:

- 5 Stories above grade
- Full basement (100% below ground)
- Approximately 93,500 sqft

Cost:

- \$40 Million



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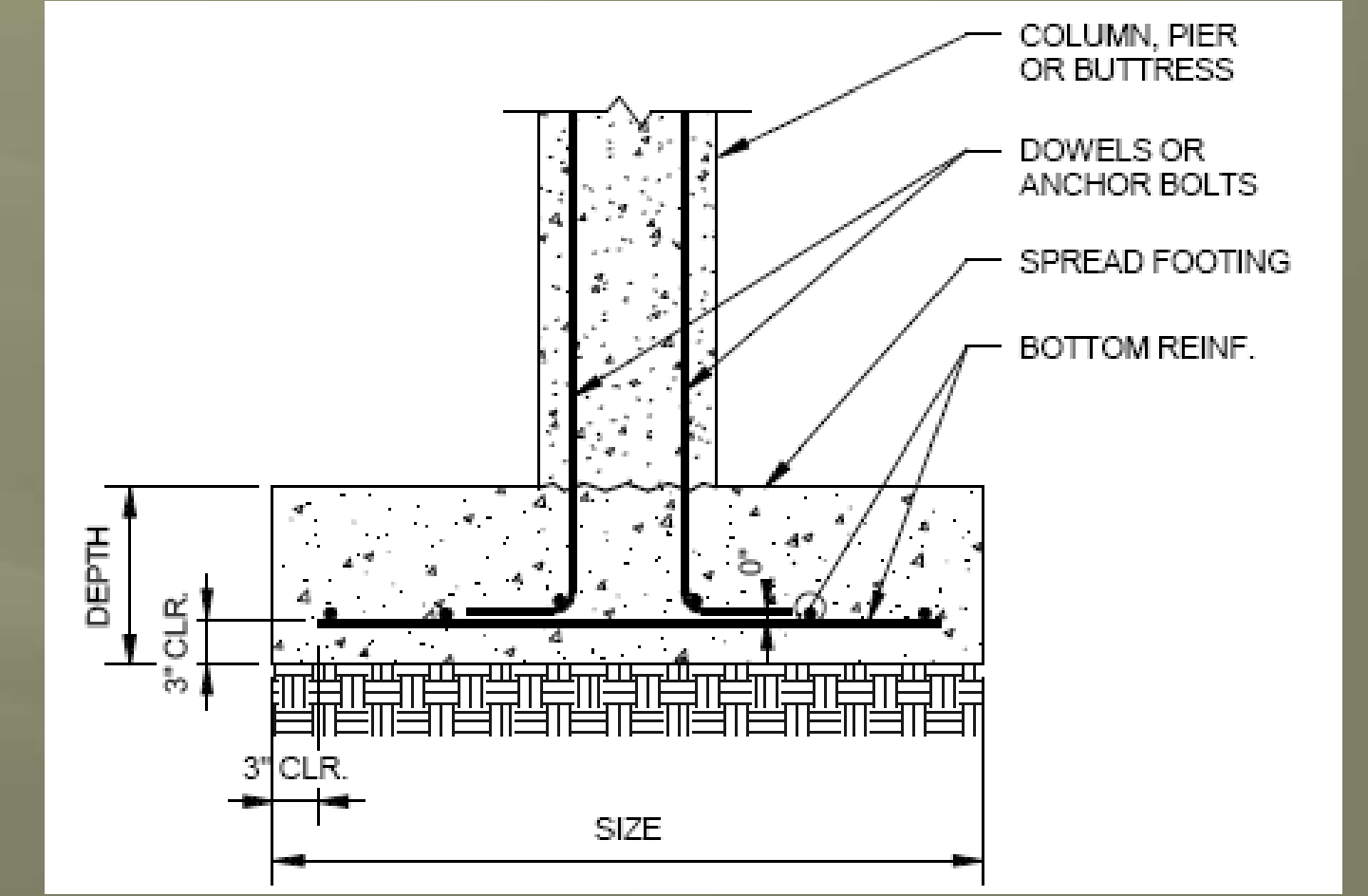
Questions & Comments

Existing Structure

Foundation System:

- Spread footing
- Sits on bedrock (15 ksi)

Typical Section



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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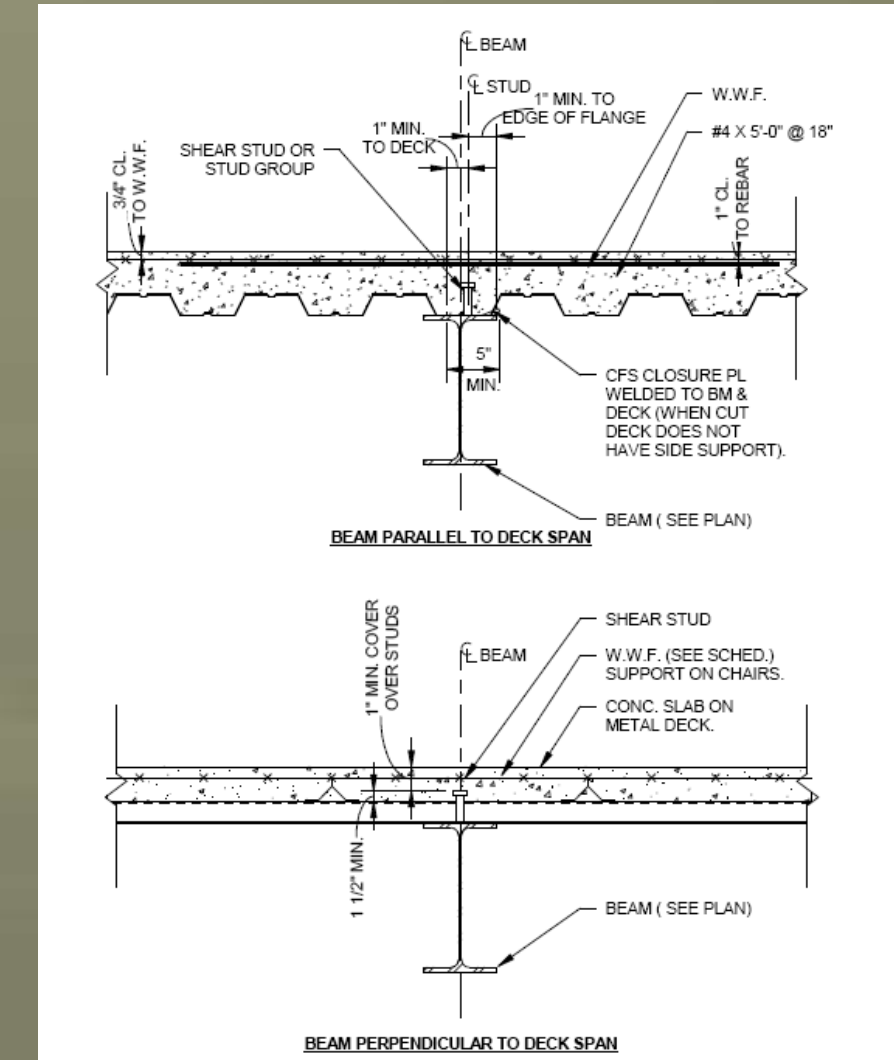
Foundation System:

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Superstructure:

- Concrete and composite metal deck

Typical Section



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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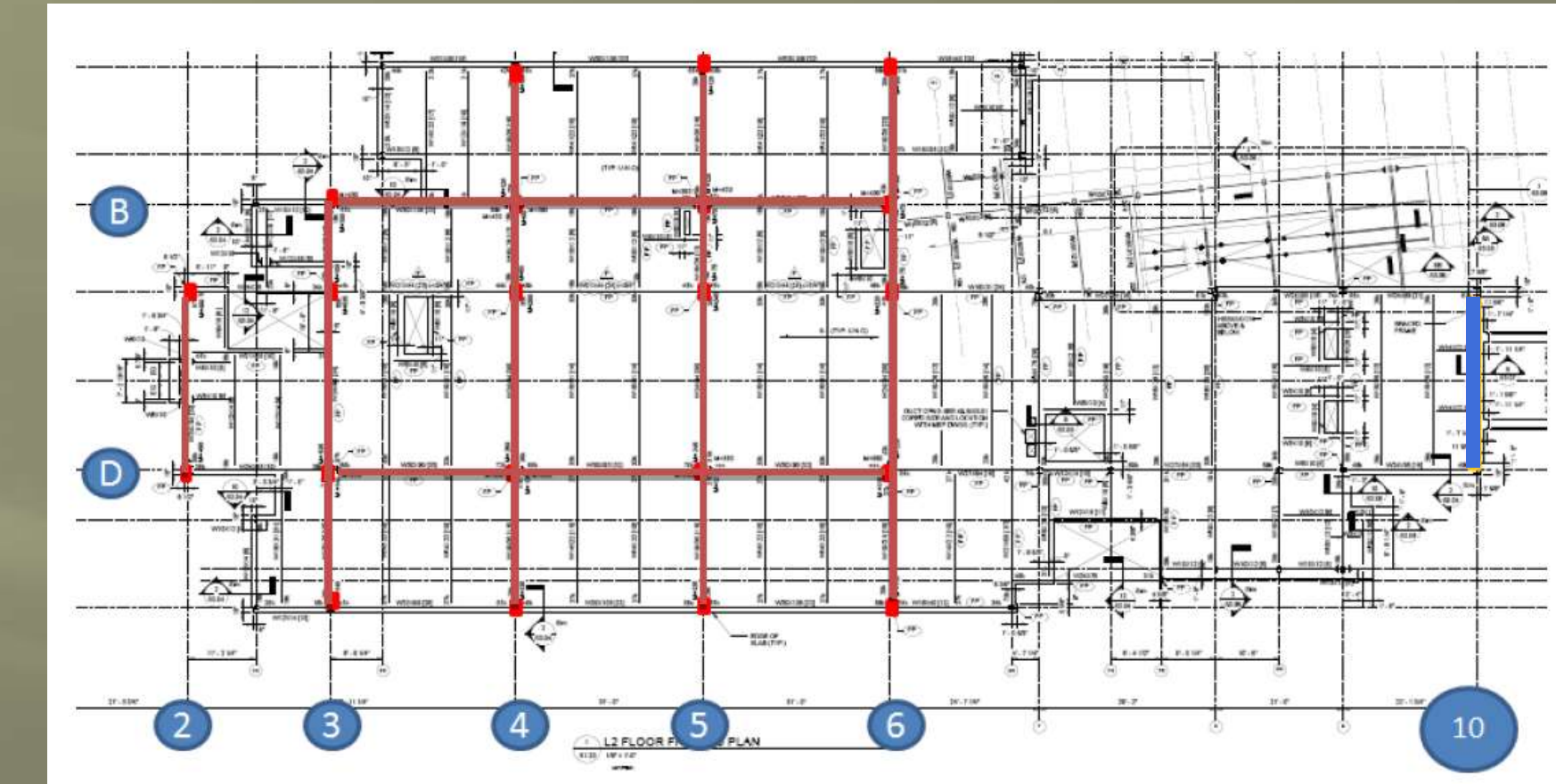
Superstructure:

- Concrete and composite metal deck

Lateral System:

- Steel Moment Frames
- Eccentric Braced Frame (Column Line 10)

Lateral Layout



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

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Schedule Impact Breadth

Conclusion

Questions & Comments

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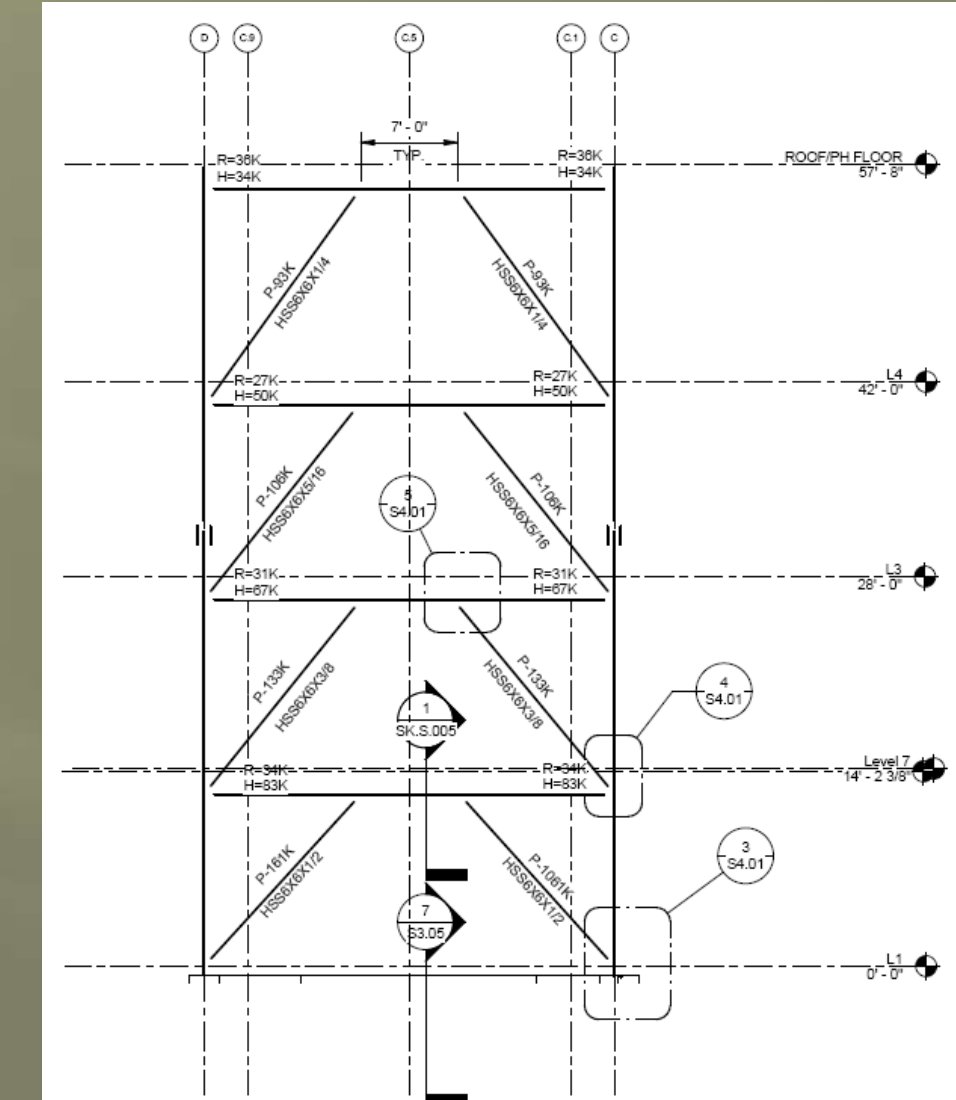
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Eccentric Braced Frame



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Problem Statement

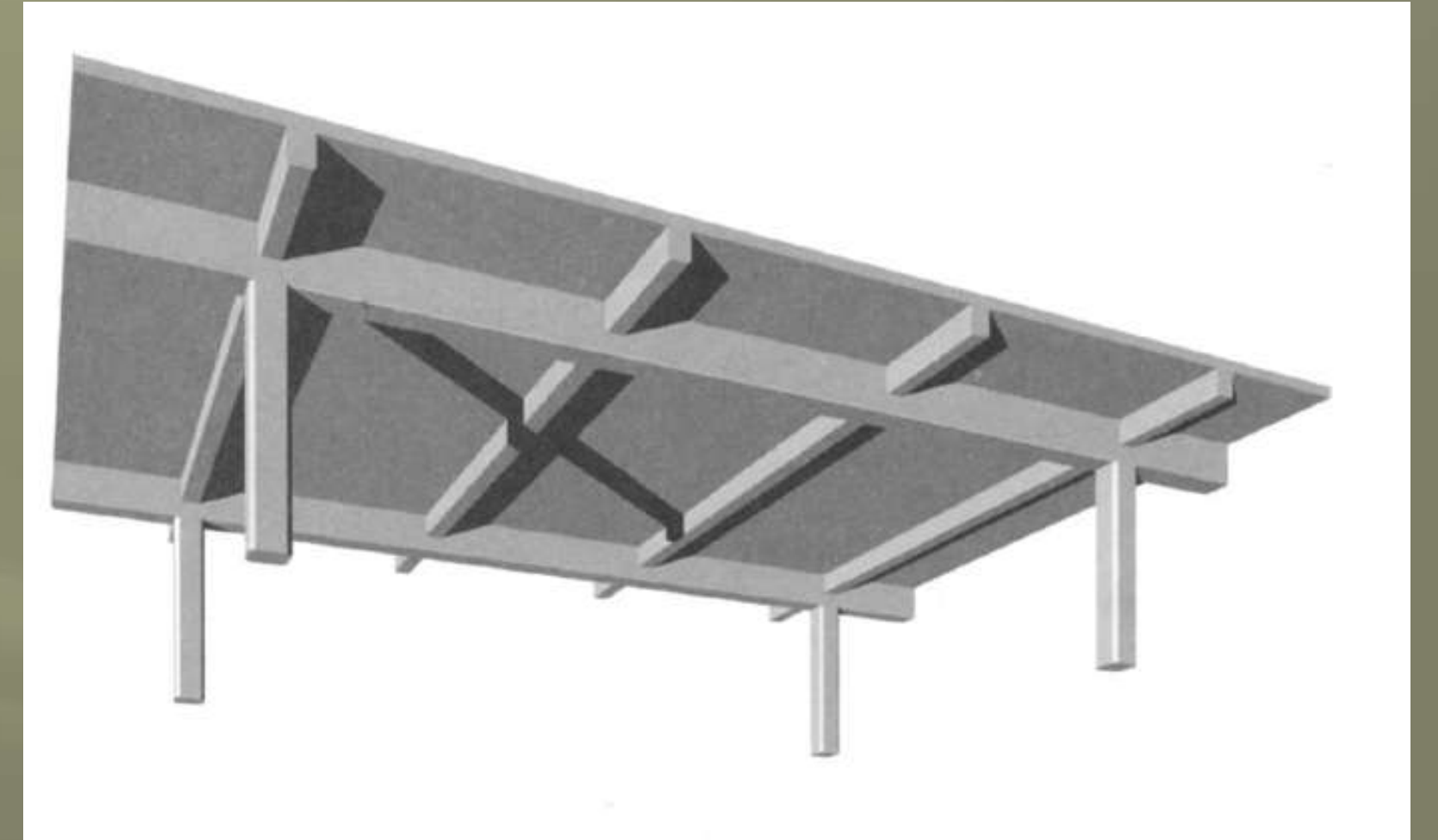
Statement:

- Steel has become an unviable option as main structural material

Solution:

Structural Depth - Redesign the structure using reinforced concrete with minimal impact on existing interior architecture and spaces

- One-way slab with interior beam
- Concrete moment frame



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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Façade Study Breadth – Change façade to precast



Presentation Outline

- Building Introduction
- Existing Structure
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- Schedule Impact Breadth
- Conclusion
- Questions & Comments

Problem Statement

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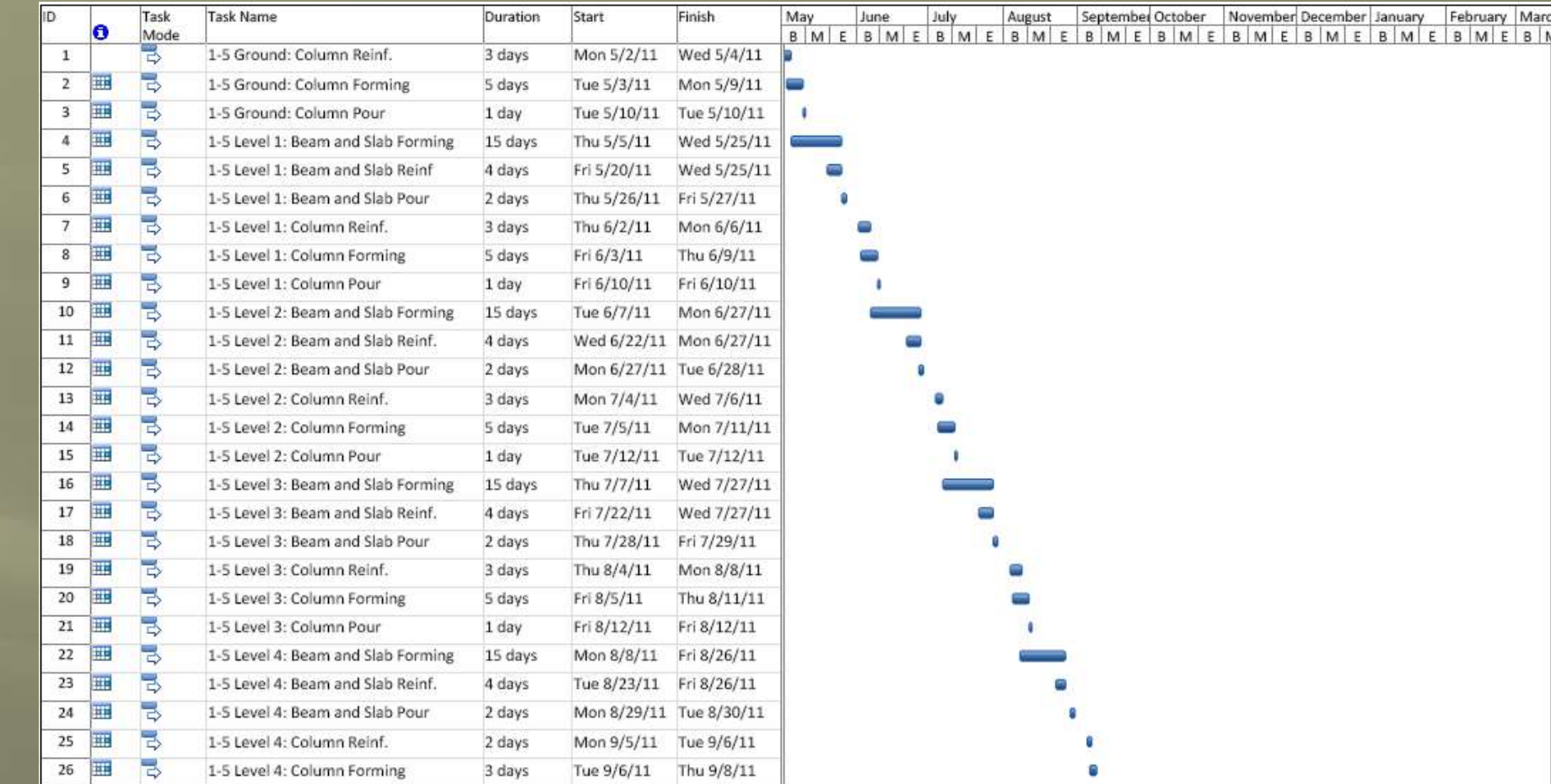
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- One-way slab with interior beam
- Concrete moment frame

Façade Study Breadth – Change façade to precast

Schedule Impact Breadth– Determine what impact the concrete redesign and precast façade have on the construction schedule



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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth - Loads

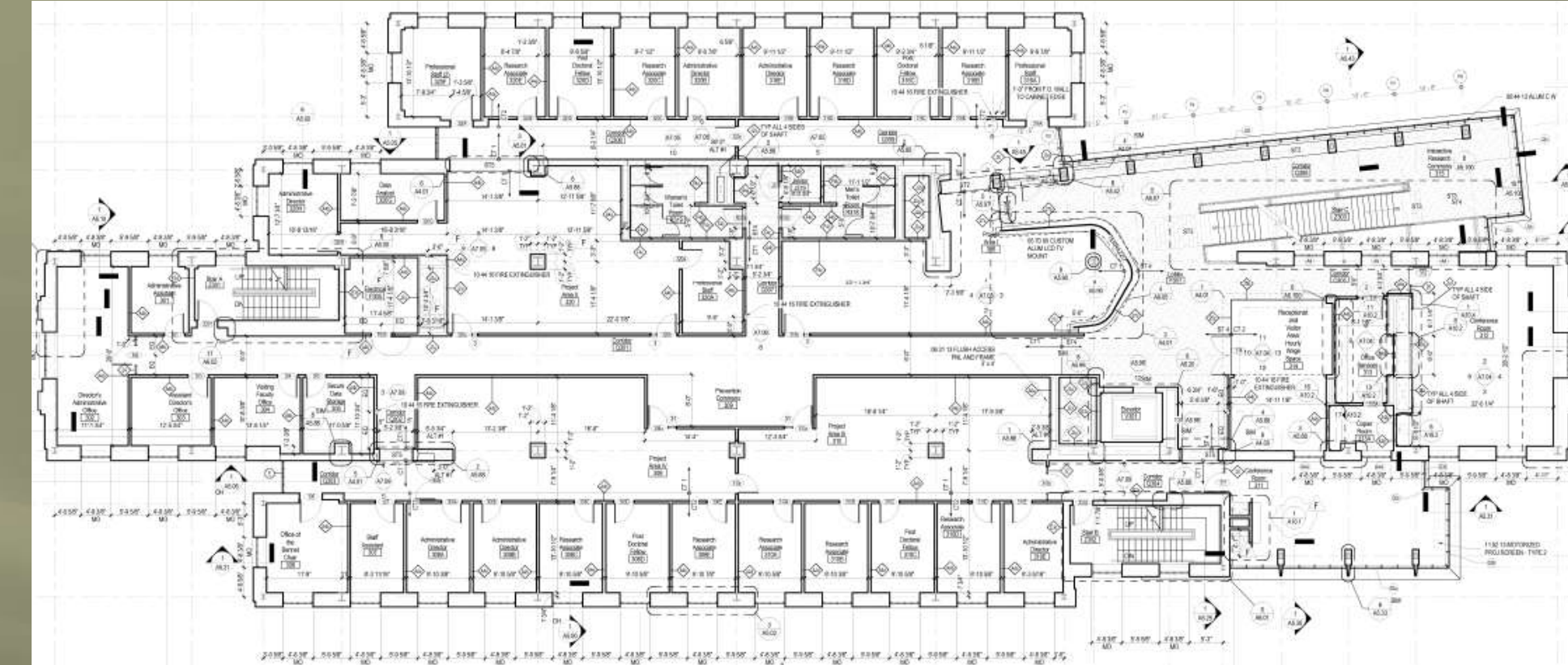
Gravity Loads:

Dead

- Structure Self weight
- Superimposed (5 psf)
- Slate Floor (20 psf)

Live

- Lobbies/Assembly (100 psf)



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth - Loads

Gravity Loads:

Dead

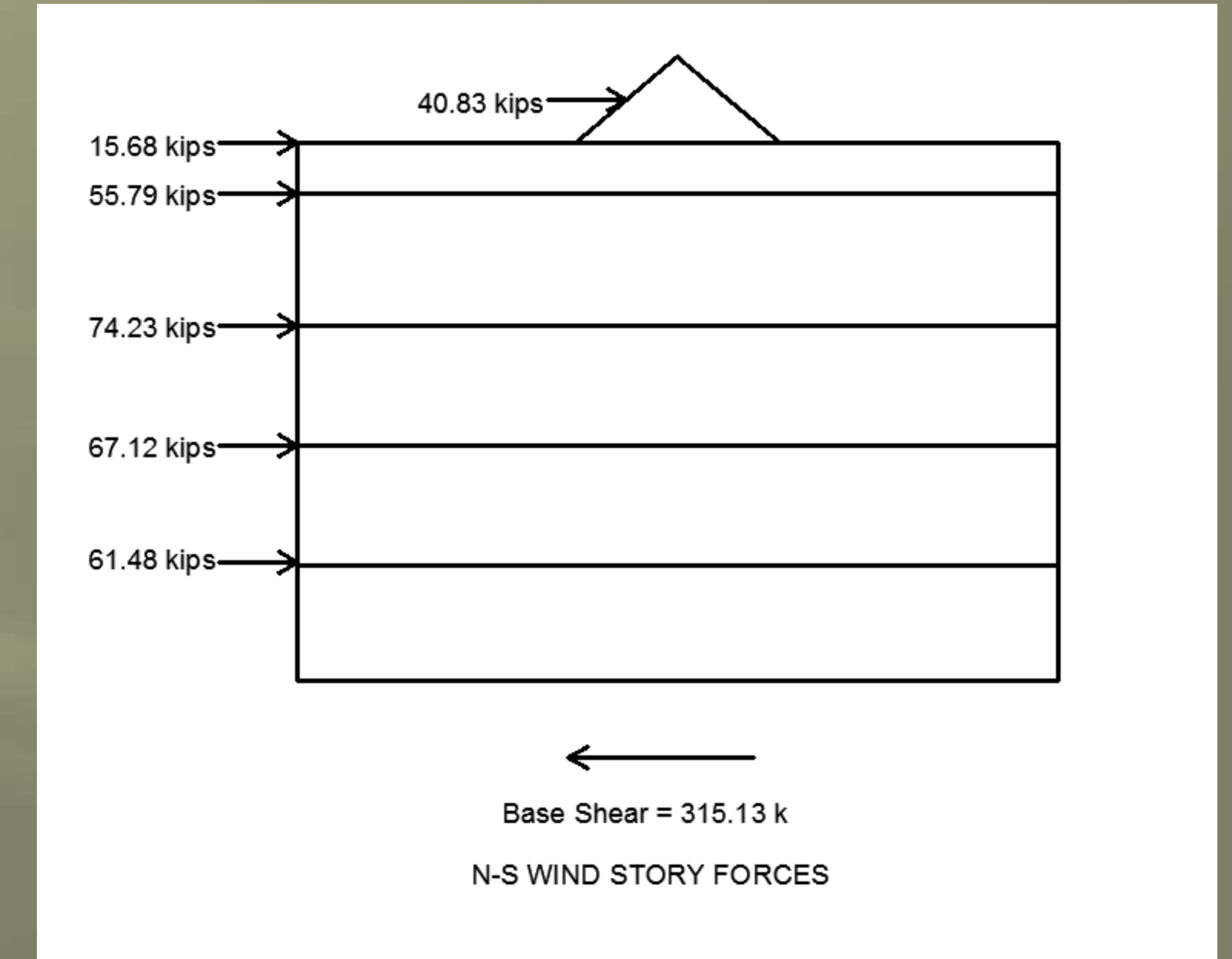
- Structure Self weight
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- Slate Floor (20 psf)

Live

- Lobbies/Assembly (100 psf)

Lateral Loads:

- Wind (Controls)
- Seismic



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

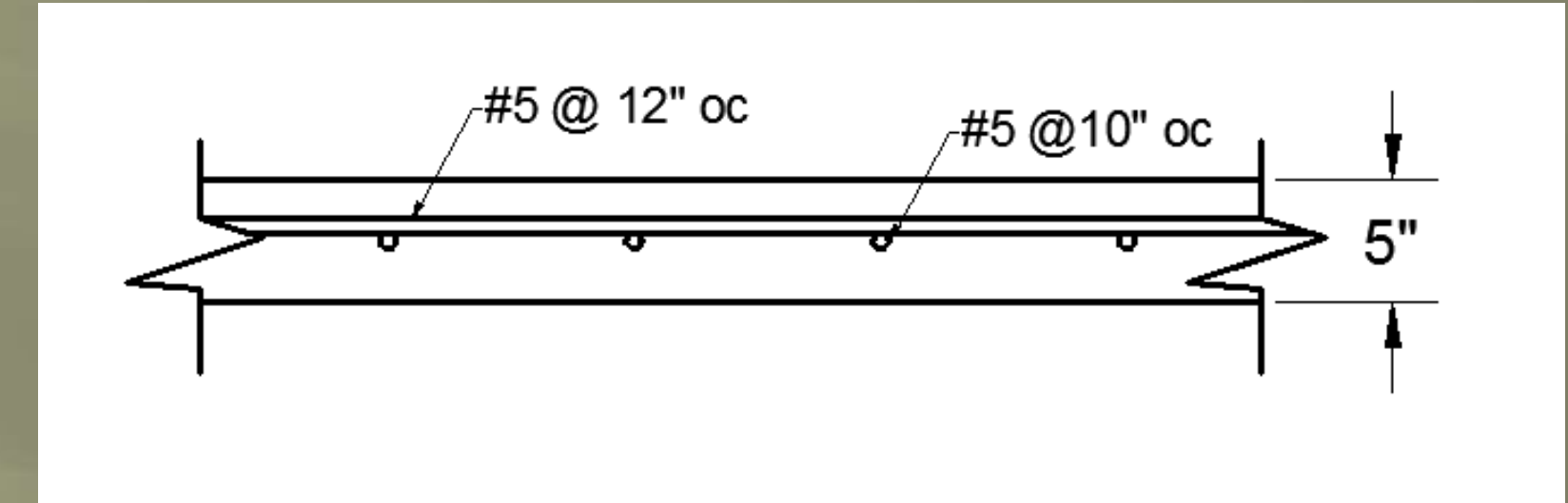
Conclusion

Questions & Comments

Structural Depth - Gravity

One-way Concrete Slab:

- 5" Slab (Table 9.5a)
- #5 @ 12" oc (flexure)
- #5 @ 10" (crack control)



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

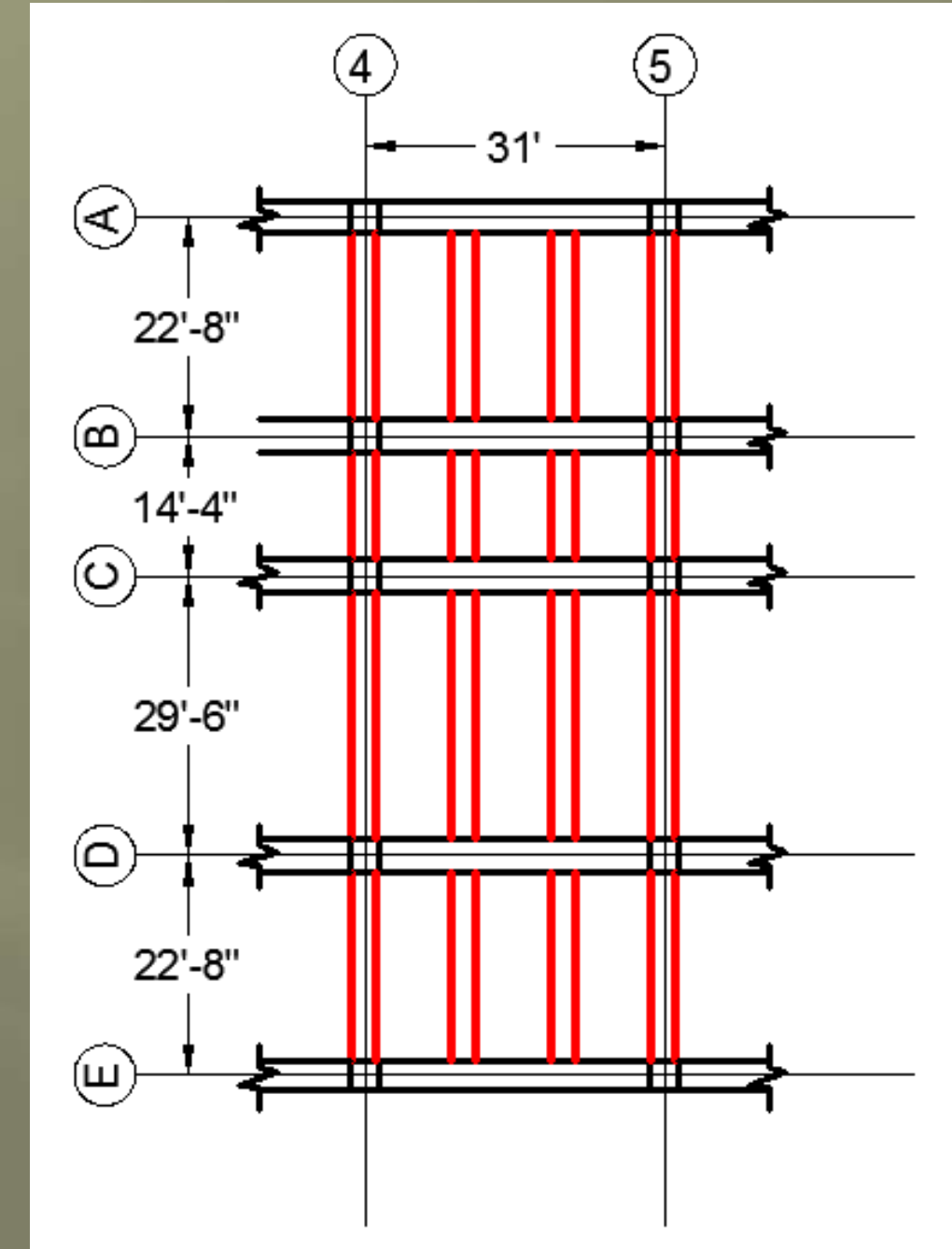
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One-way Concrete Slab:

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- #5 @ 12"oc (flexure)
- #5 @ 10" (crack control)

Beams :

- Support slab
- Run N-S
- Supported by girders, edge beams, & Columns
- Flexure & shear controlled design
- #5 in corners for cage construction
- Consistent concrete cross section



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

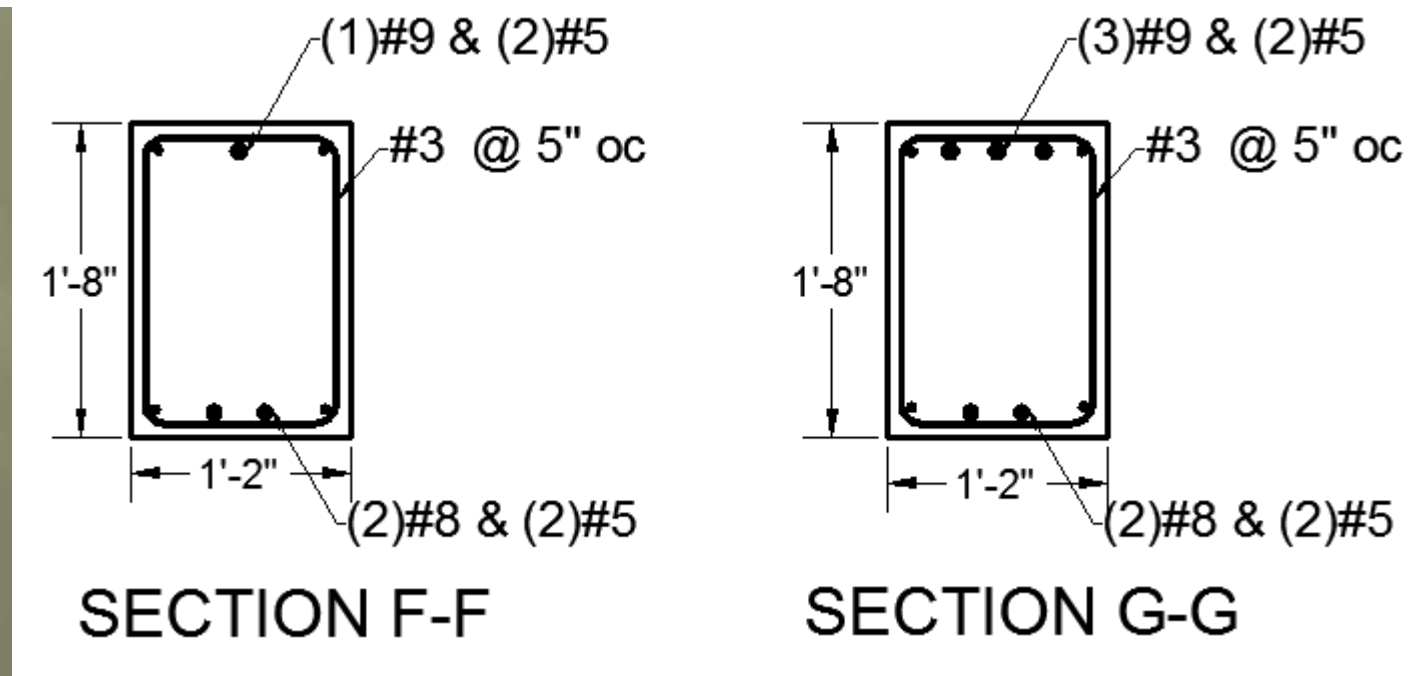
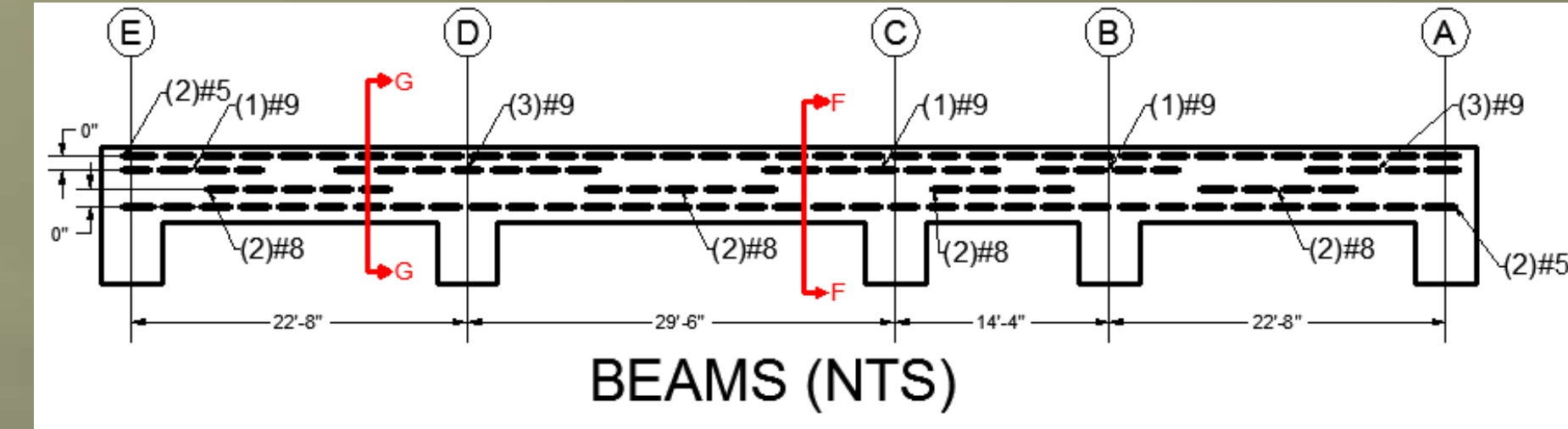
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Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

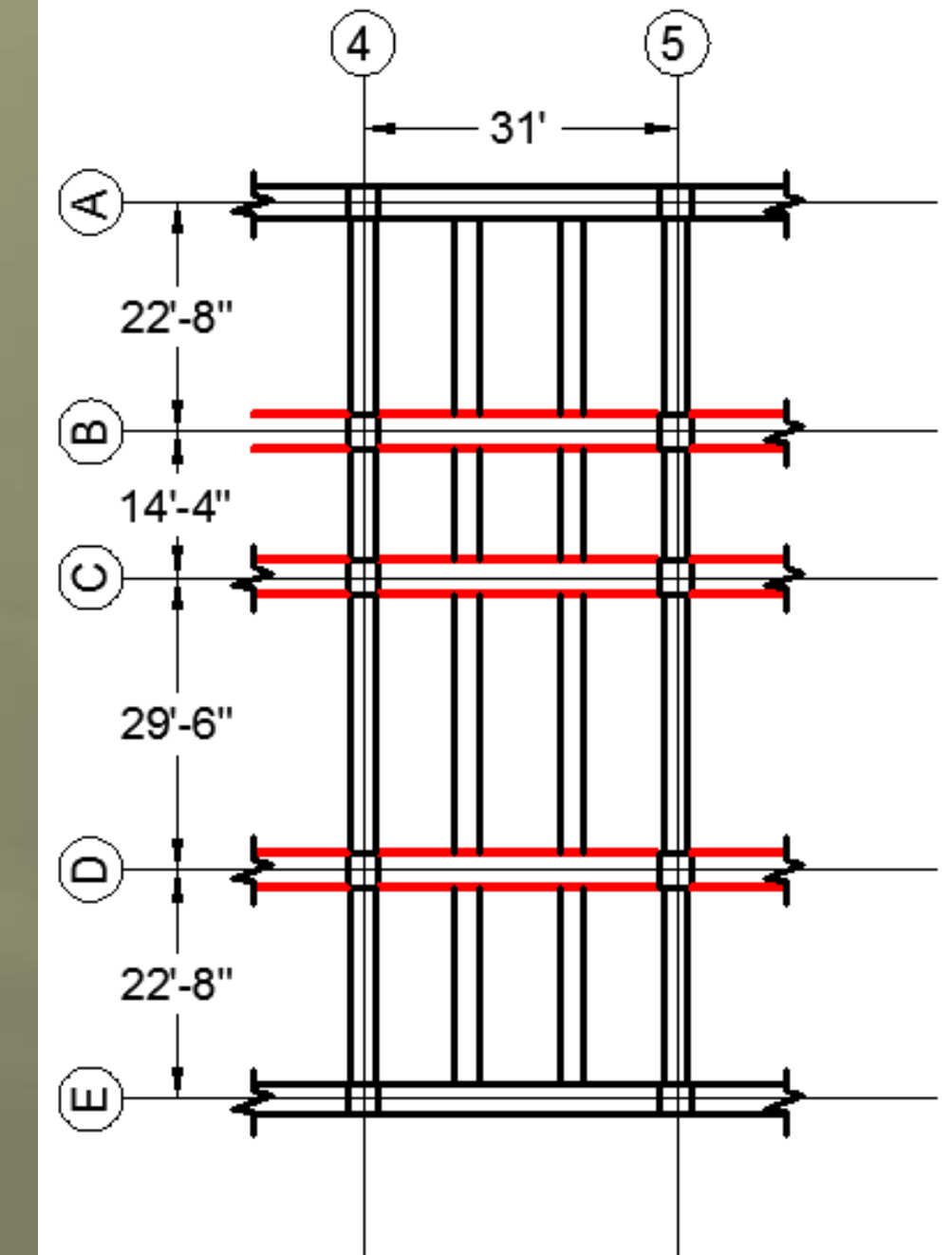
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Questions & Comments

Structural Depth - Gravity

Girders:

- Run E-W
- Supported by columns at both ends
- Concentrated loads produce large moments
- 2" shallower than existing steel structure
- Assumed 50% sustained live load for deflections



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

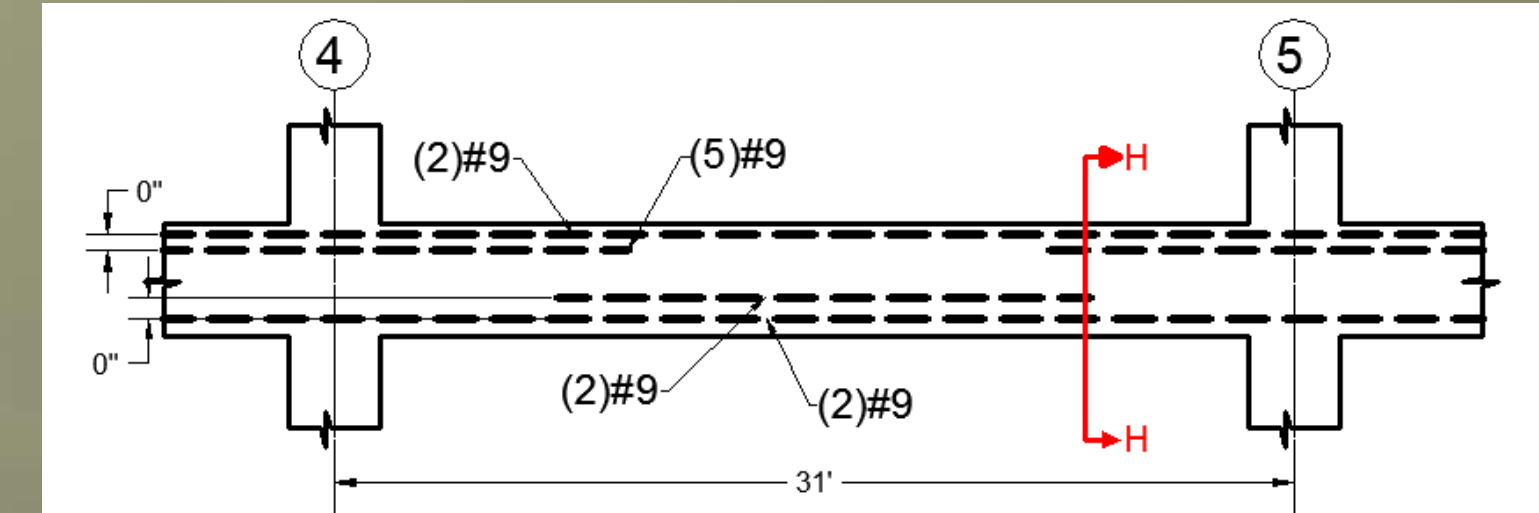
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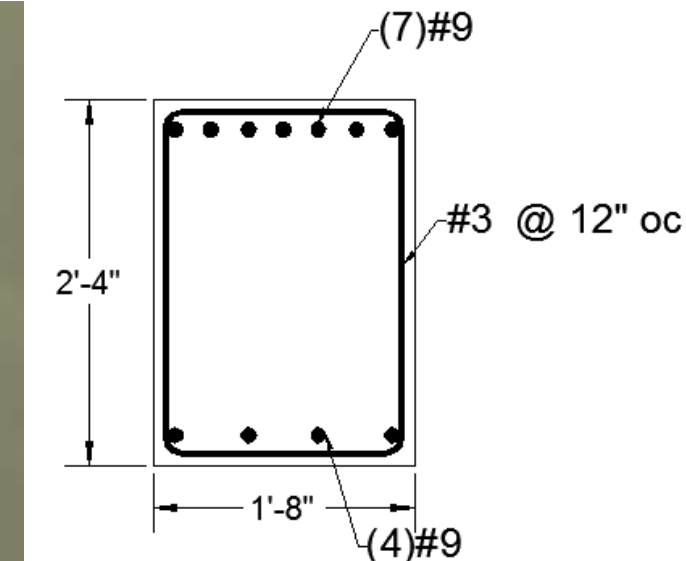
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GIRDER (NTS)



SECTION H-H

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Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

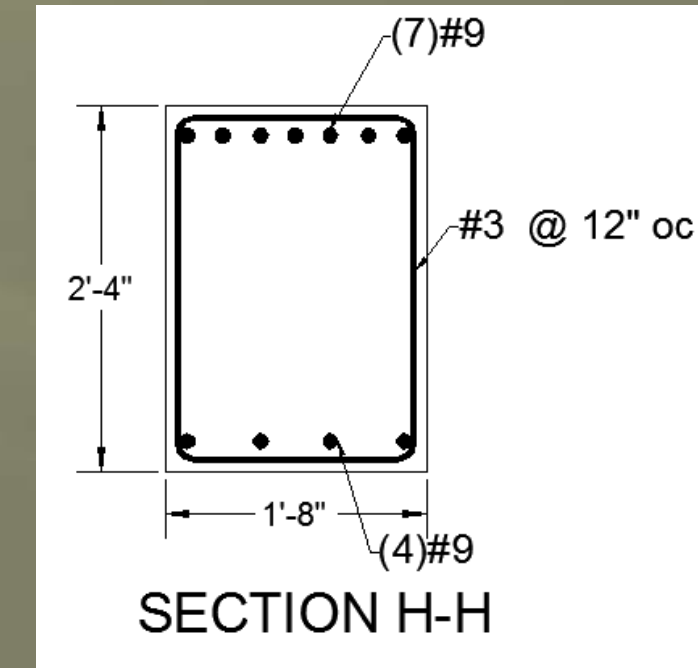
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Girder Deflections			
	Actual	Allowable	Pass?
$\Delta i(d+l)$	0.11 in	L/240 1.55 in	Yes
$\Delta i(\text{live})$	0.06 in	L/360 1.03 in	Yes
Δlong	0.2 in	L/240 1.55 in	Yes



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

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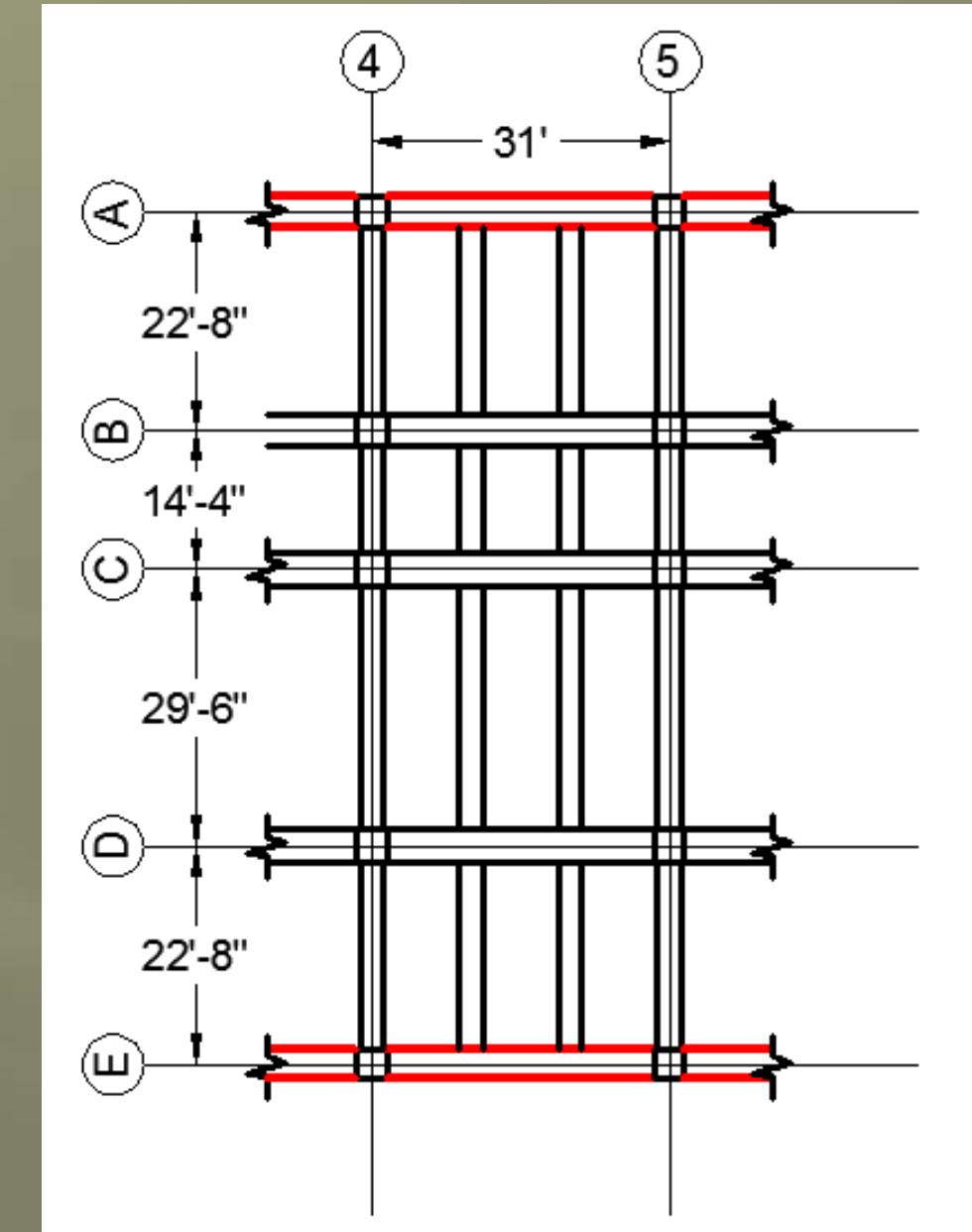
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Girders:

- Run E-W
- Supported by columns at both ends
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Edge Beam:

- Run perimeter of BBH Building
- Concentrated load produces torsion
 - Added longitudinal & transverse reinforcement
- Supports masonry



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

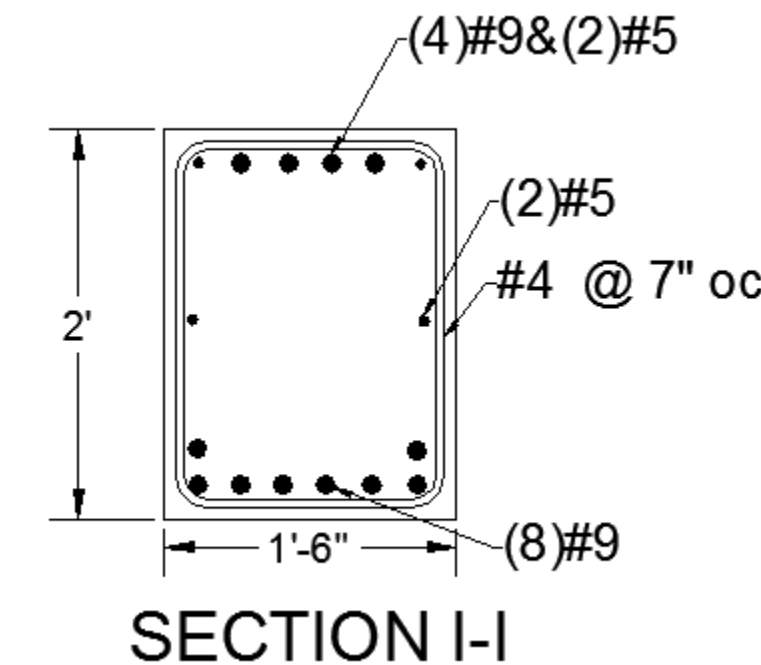
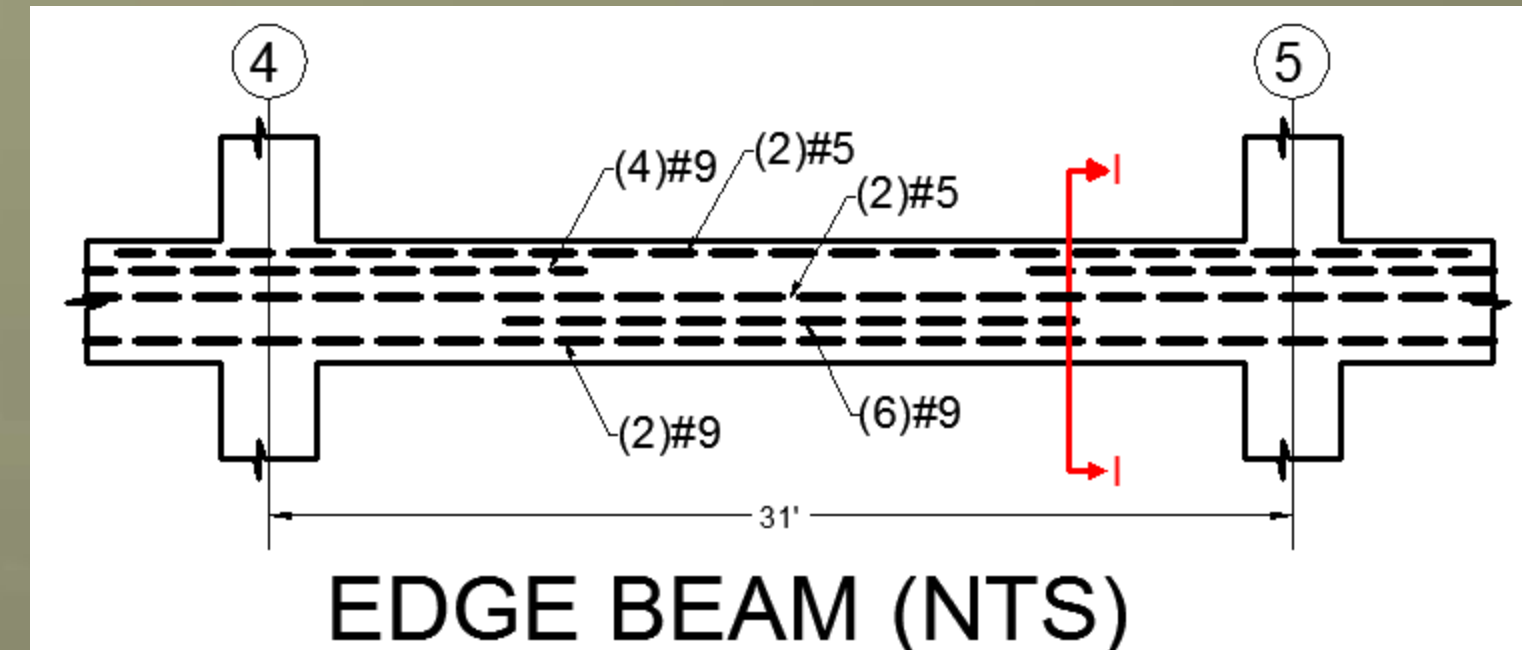
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Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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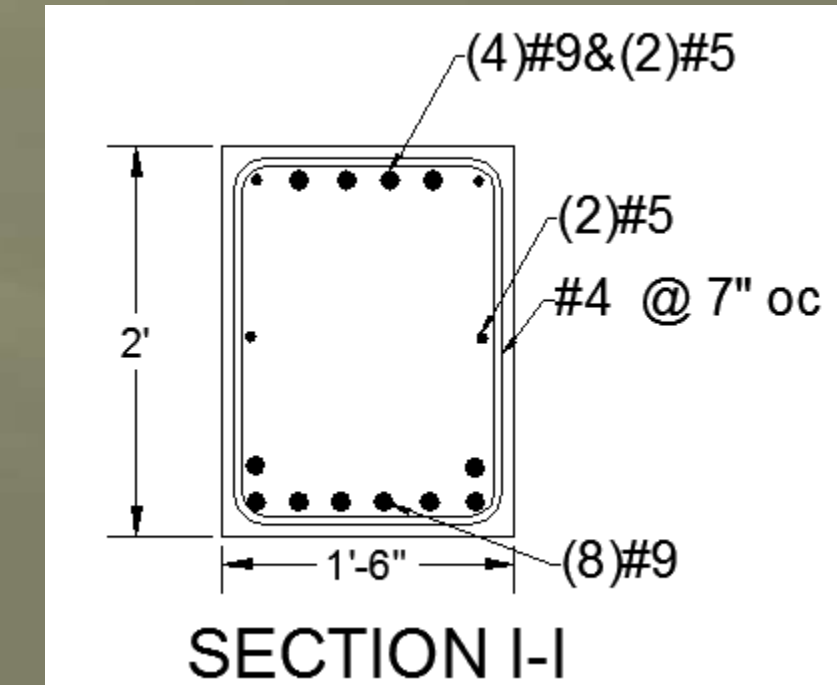
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Edge Beam:

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- Supports masonry

Edge Beam Deflections				
	Computed	Allowable		Pass?
$\Delta i(d+l)$	0.29 in	L/600	0.62 in	Yes
$\Delta i(\text{live})$	0.06 in	L/360	1.03 in	Yes
Δlong	0.58 in	L/600	0.62 in	Yes



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth - Lateral

Concrete Moment Frame:

- Does not affect interior architecture.
- Stiff beam to column connection



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

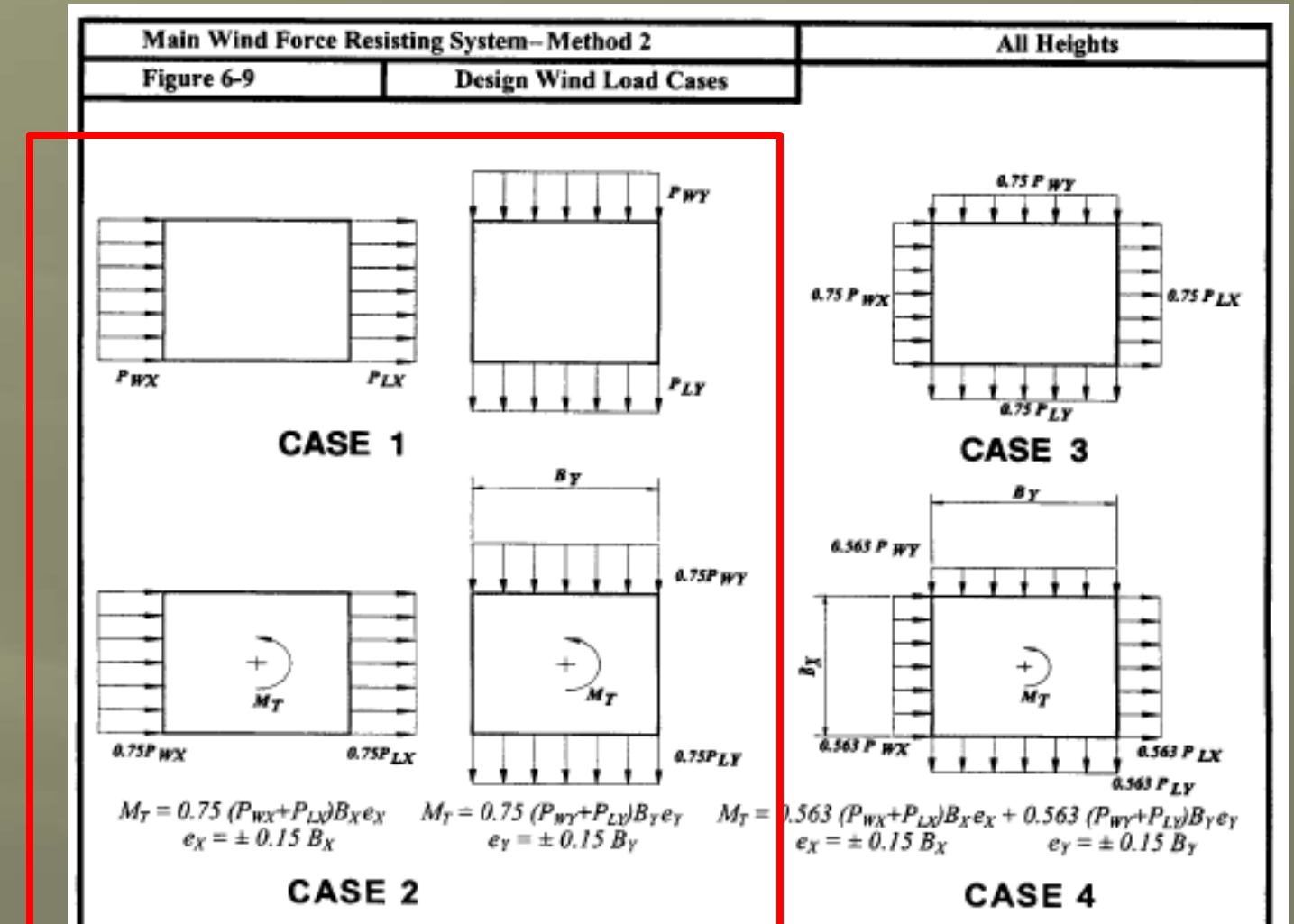
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Wind Loads:

- Case 1 & Case 2 Controlled



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth - Lateral

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Wind Loads:

- Case 1 & Case 2 Controlled

Relative Stiffness:

- 1 kip load applied to each frame
- Calculated relative stiffness based on deflection.
- Distribution of wind loads

Frame	K (k/in)	ΣK_{NS} (k/in)	ΣK_{EW} (k/in)	Direct shear (kip)	d (in)	Kd ²	ΣKd^2	Torsional Moment Shear (kip)	Total shear (kip)
B	0.5502	0.00	4.23	0.00	32.50	581.15	17444.38	1.04	1.04
C	1.2902	0.00	4.23	0.00	18.20	427.38	17444.38	1.36	1.36
D	1.3881	0.00	4.23	0.00	-11.30	177.25	17444.38	-0.91	-0.91
E	1.0000	0.00	4.23	0.00	-34.00	1156.00	17444.38	-1.97	-1.97
1	0.1972	3.51	0.00	6.32	-106.00	2215.32	17444.38	-1.21	5.10
2	0.2560	3.51	0.00	8.20	-84.70	1836.50	17444.38	-1.26	6.94
3	0.3437	3.51	0.00	11.01	-61.30	1291.35	17444.38	-1.22	9.79
4	0.4860	3.51	0.00	15.57	-30.70	458.02	17444.38	-0.86	14.70
5	0.5848	3.51	0.00	18.73	0.30	0.05	17444.38	0.01	18.74
6	0.5309	3.51	0.00	17.00	31.30	520.08	17444.38	0.96	17.97
7	0.4180	3.51	0.00	13.39	55.90	1306.04	17444.38	1.35	14.74
8	0.2922	3.51	0.00	9.36	85.00	2111.43	17444.38	1.44	10.80
9	0.2248	3.51	0.00	7.20	106.00	2525.70	17444.38	1.38	8.58
10	0.1727	3.51	0.00	5.53	128.20	2838.10	17444.38	1.28	6.81

Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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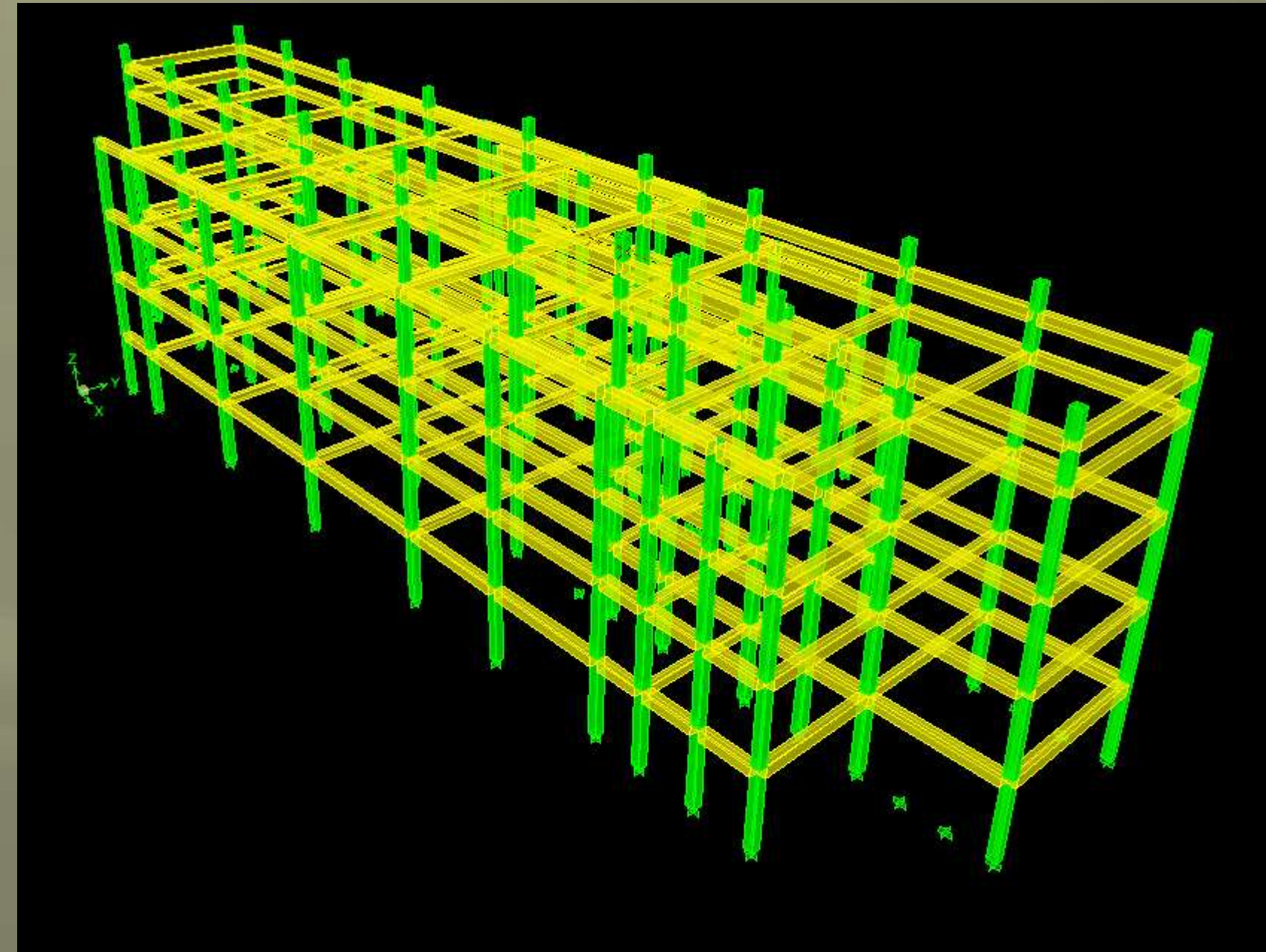
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Relative Stiffness:

- 1 kip load applied to each frame
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ETABS:

- Line elements with proper material & section properties
- Columns – $0.70 \cdot I_g$
- Beams – $0.35 \cdot I_g$
- Verified output with hand calculations



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

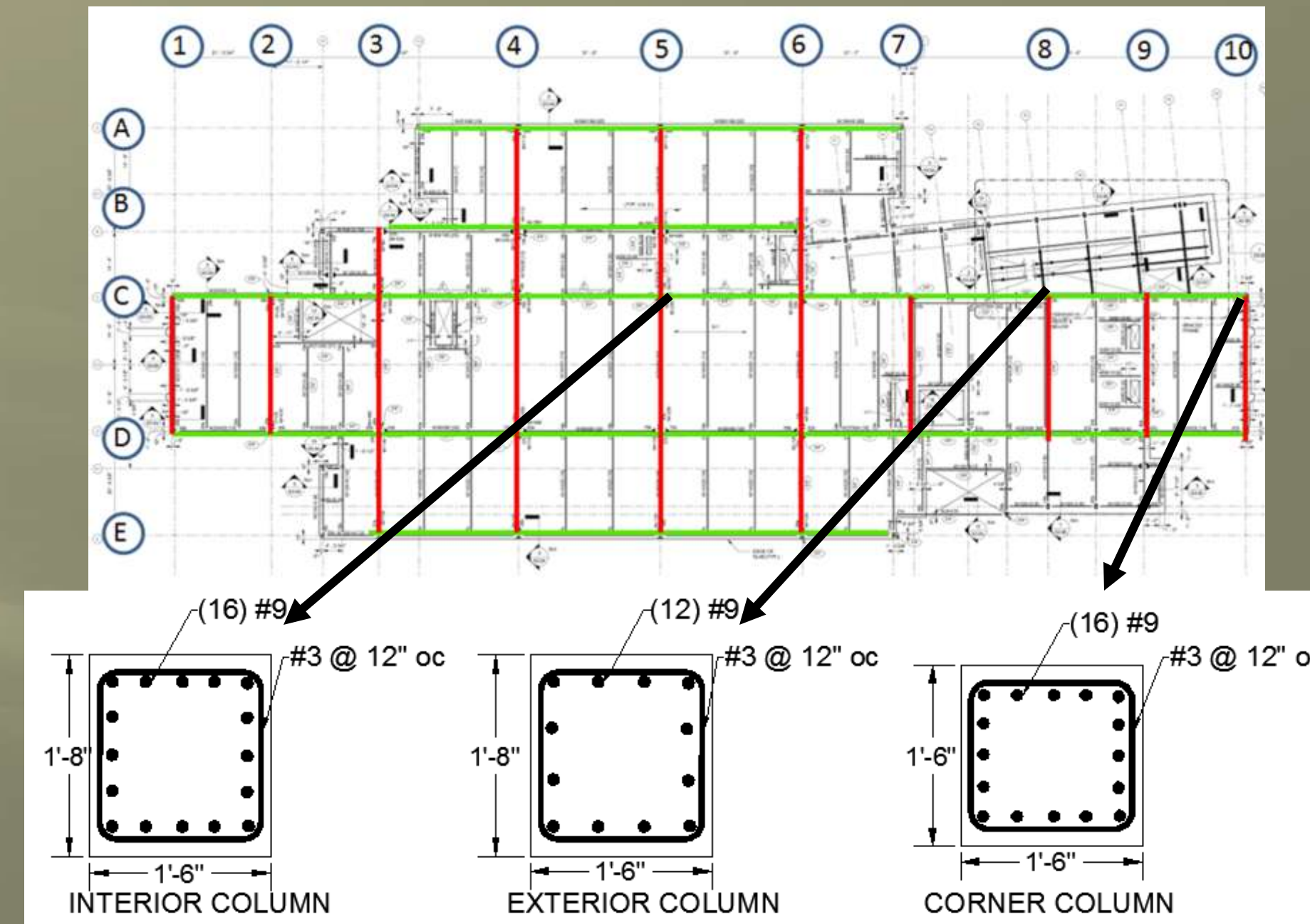
Conclusion

Questions & Comments

Structural Depth - Lateral

Column Design:

- Corner, Interior, & Exterior
- Resists axial & flexural loads



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth - Lateral

Column Design:

- Corner, Interior, & Exterior
- Resists axial & flexural loads

Design Checks:

- Lateral Displacement < H/400
 - $0.9D+L+W$

Displacement - X Direction					
Story	Height	Story Height	Displacement	H/400	Pass?
	(ft)	(ft)	(in)	(in)	Yes
PH	57	15	0.18	1.71	Yes
4	42	14	0.15	1.26	Yes
3	28	14	0.11	0.84	Yes
2	14	14	0.05	0.42	Yes
Displacement - Y Direction					
Story	Height	Story Height	Displacement	H/400	Pass?
	(ft)	(ft)	(in)	(in)	Yes
PH	57	15	1.6	1.71	Yes
4	42	14	1.25	1.26	Yes
3	28	14	0.82	0.84	Yes
2	14	14	0.31	0.42	Yes

Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Structural Depth – Cost Impact

Steel		Concrete	
Structural steel	\$297,025	Beams	\$220,000
Metal Deck	\$49,345	Columns	\$94,504
1" Spray on Fireproofing	\$12,968	Slab	\$141,000
Concrete fill	\$48,183	Total	\$455,504
Total	\$407,521		
% increase	12%		
Cost Diff	\$47,984		

Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

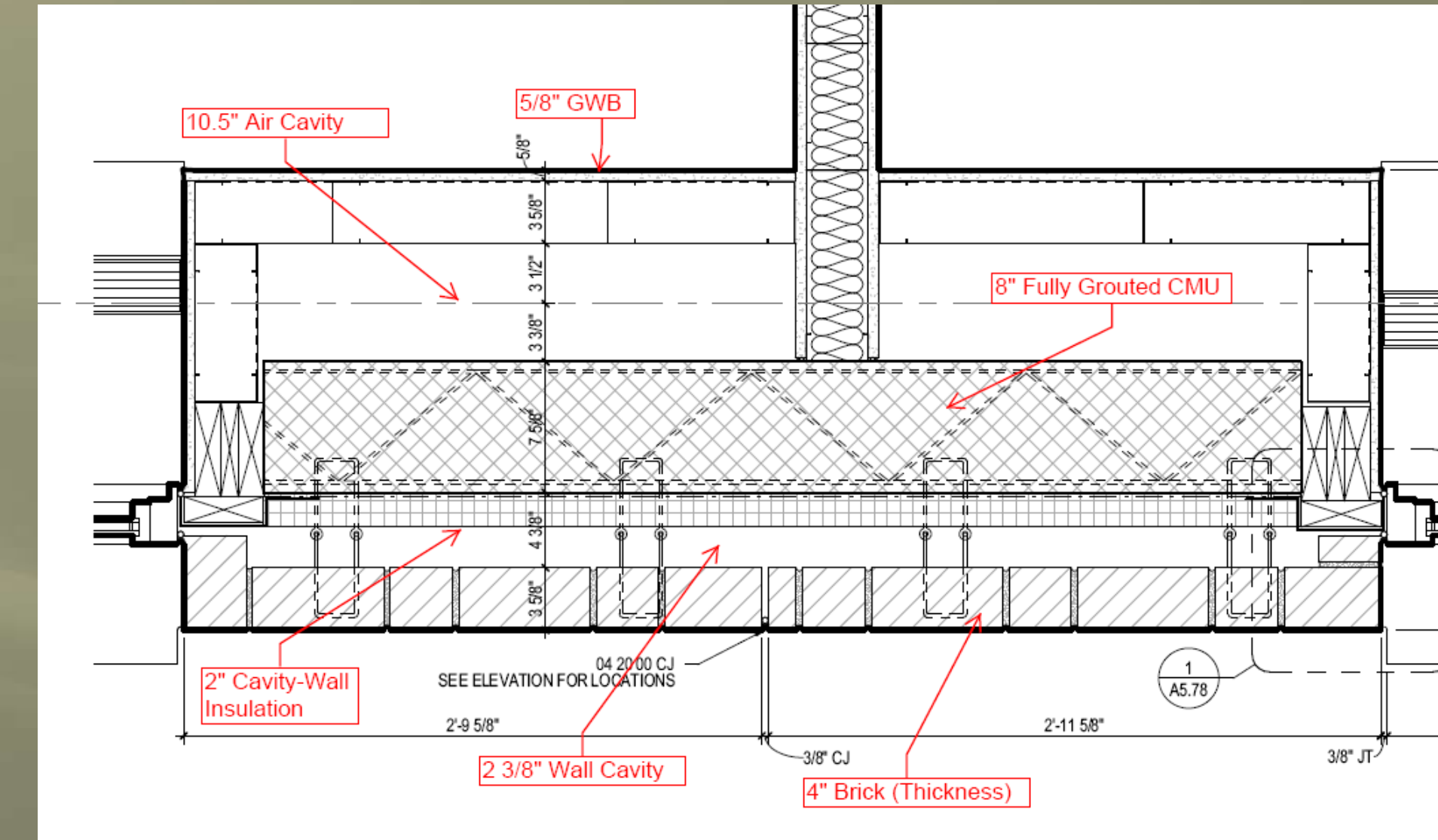
Conclusion

Questions & Comments

Façade Study Breadth

Existing Façade:

- Traditional hand placed brick & limestone
- Held back by 8" fully grouted CMU
- Flashing, weep holes, & air barrier
- Heavy & Expensive



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

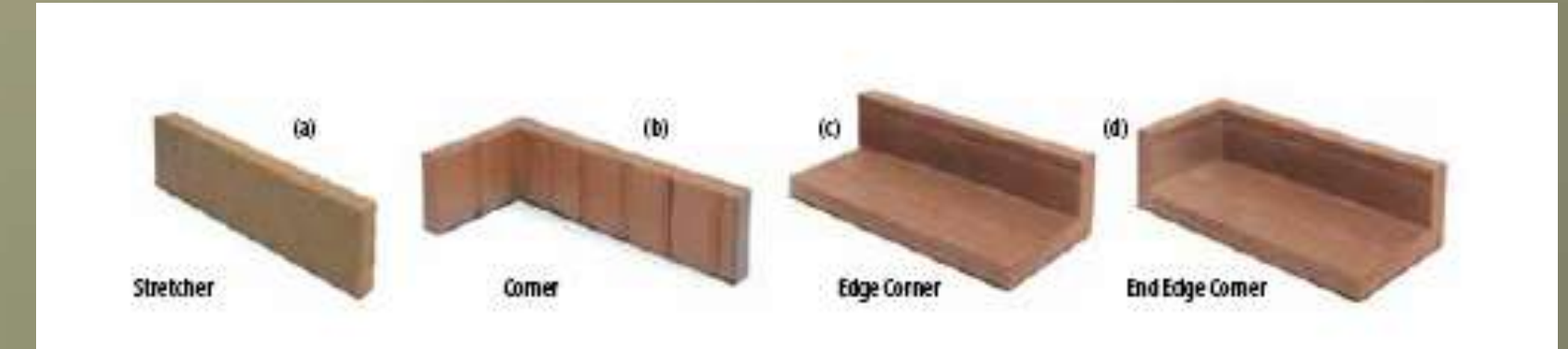
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- Traditional hand placed brick & limestone
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- Flashing, weep holes, & air barrier
- Heavy & Expensive

Alternative Façade:

- Thin brick precast panels
- Made in controlled conditions
- Faster Construction



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

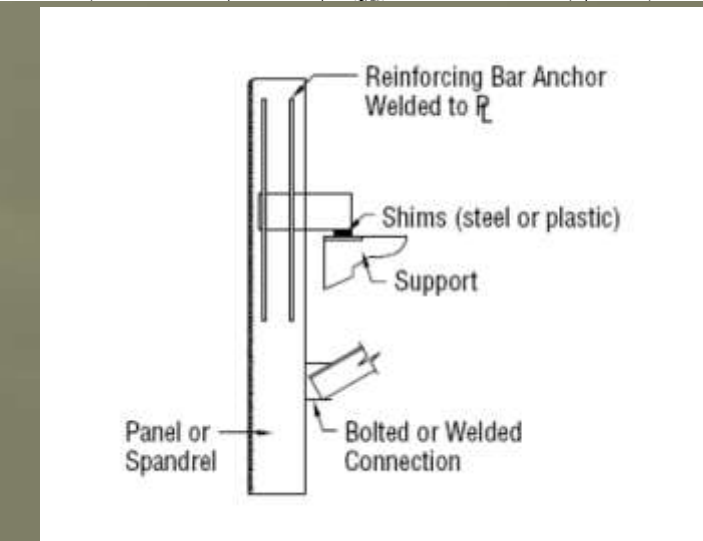
Conclusion

Questions & Comments

Façade Study Breadth

Thin Brick Precast:

- Typical Layout
- Hung from edge beams
- Kickback provide lateral support



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

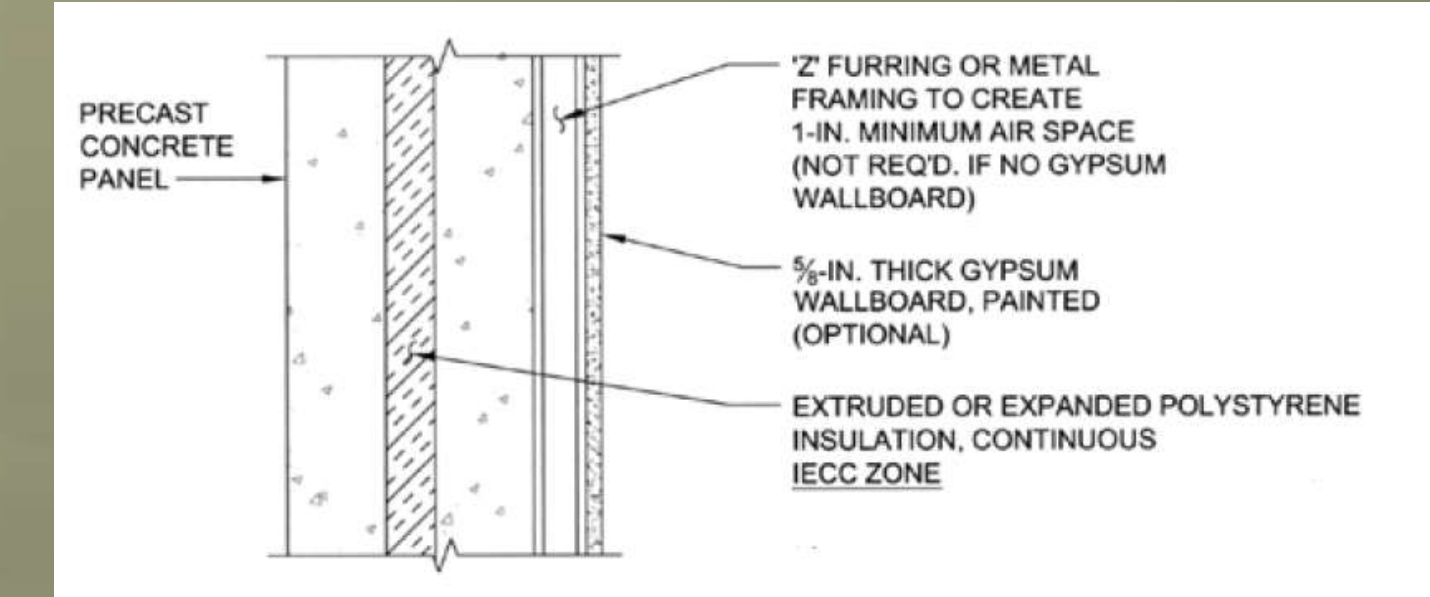
Façade Study Breadth

Thin Brick Precast:

- Typical Layout
- Hung from edge beams
- Kickback provide lateral support

Thermal & Moisture Resistance:

- Sandwich Wall
 - Provides rain barrier & thermal resistance



Existing Wall			Precast Wall		
Material	Thickness (in)	R-Value	Material	Thickness (in)	R-Value
Brick	4	0.4	Thin Brick	1	0.1
Air Cavity	2.375	1	Sandwich Panel Walls	4	4.4
Rigid Insulation	2	4.35	Air Cavity	18.5	1
Fully Grouted CMU	8	2.3	Wall Insulation Between Studs(Total R=13)	4	5.1
Air Cavity	10.5	1	GWB	0.625	0.45
GWB	0.625	0.45	Total Resistance		11.05
Total Resistance		9.5			

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Façade Study Breadth

Cost Impact:

Traditional Masonry		Precast Panels	
Brick	\$156,142	Brick	\$336,938
CMU	\$86,289	Cornice	\$81,250
Cleaning & Repointing	\$57,526	Total	\$418,188
Grouting	\$152,185		
Reinf	\$8,000		
Scaffolding	\$12,500		
Total	\$472,642		
% decrease	40%		
Cost Diff	\$54,454		

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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

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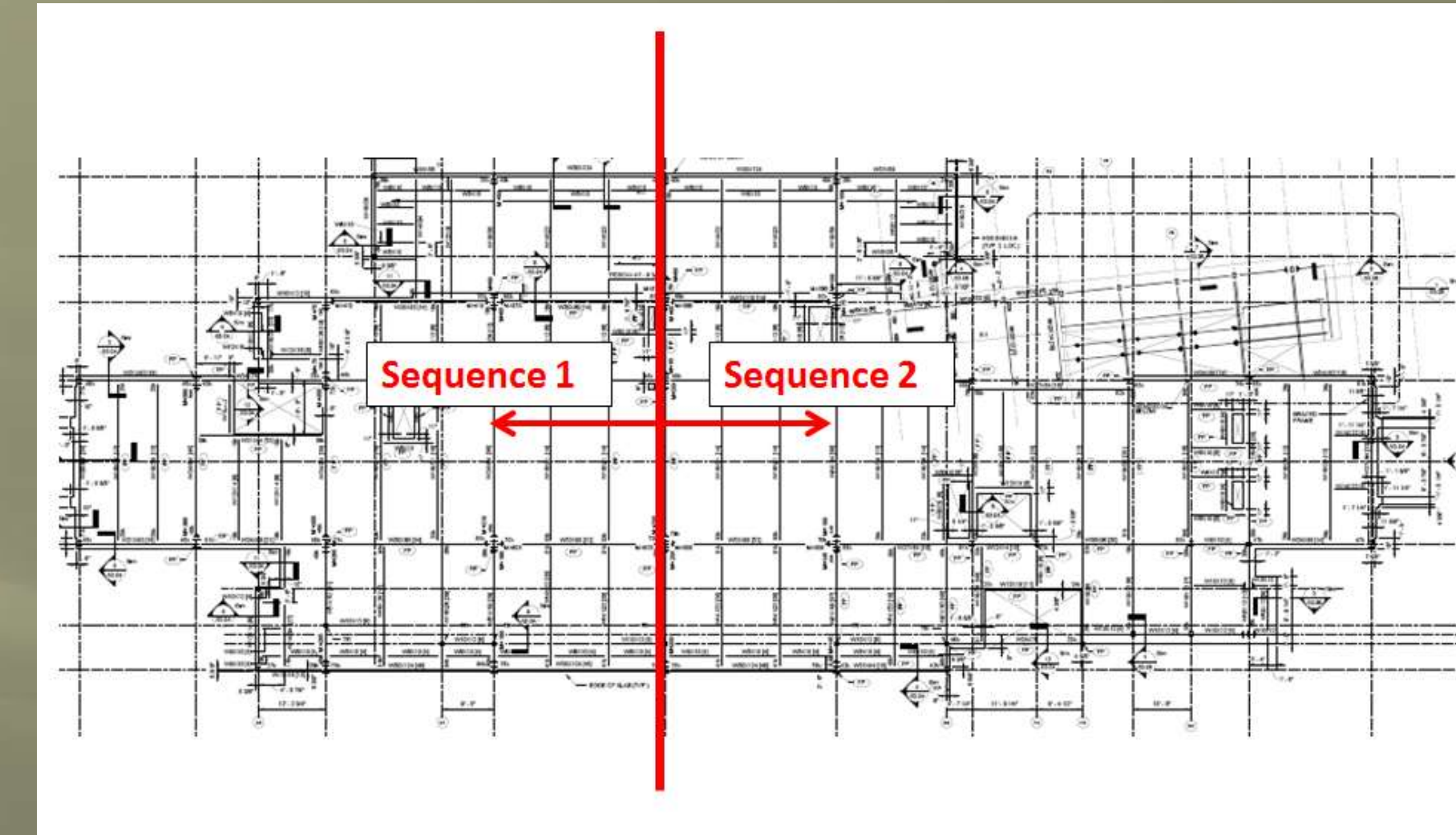
Conclusion

Questions & Comments

Schedule Impact Breadth

Construction Sequencing:

- Sequence 1: Col Line 1-5
- Sequence 2: Col Line 5-10



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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

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Conclusion

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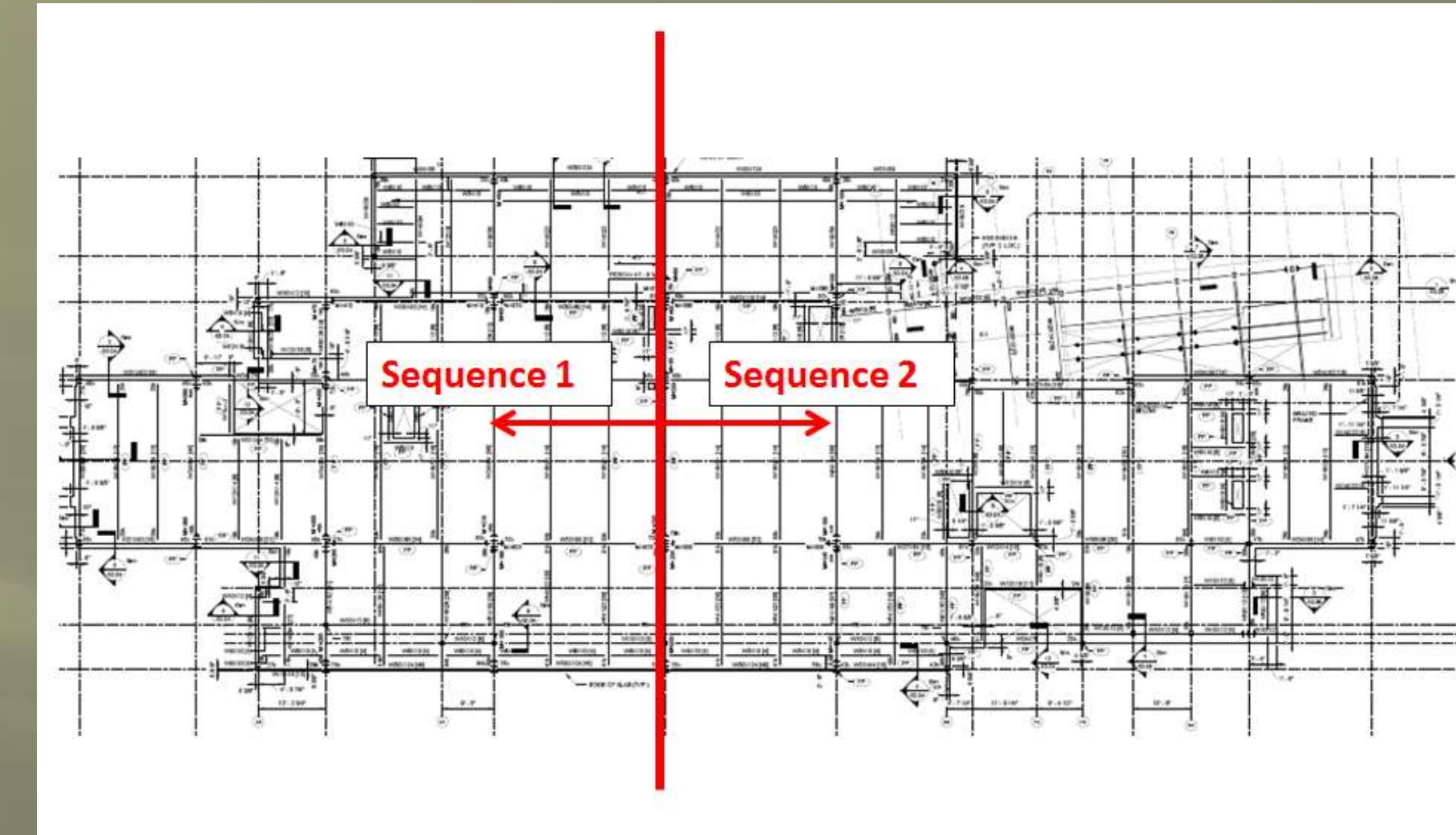
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Construction Sequencing:

- Sequence 1: Col Line 1-5
- Sequence 2: Col Line 5-10

Assumptions:

- Reinforcement starts 1-3 days after forming starts
- Wait 7 days for concrete cure before construction on next floor



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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

Schedule Impact Breadth

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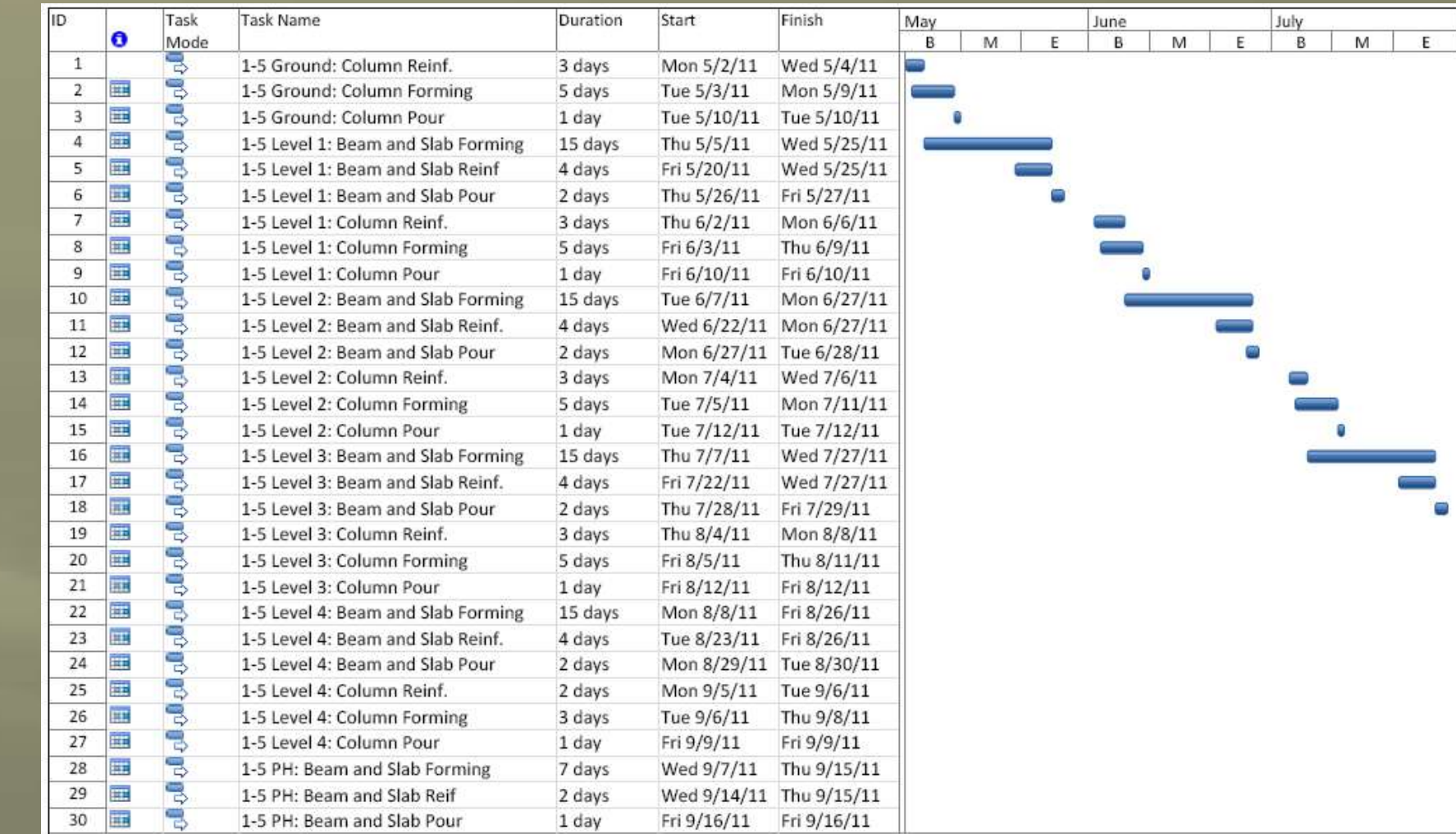
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Assumptions:

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Key Completion Dates:

- Concrete redesign: Feb 3, 2012 (+3 months)
- Alternative precast façade: Mar. 15, 2012 (-6 months)



Presentation Outline

Building Introduction

Existing Structure

Problem Statement

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Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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Structural Depth;

- Successful concrete redesign
- Met all serviceability requirements
- Minimal impact interior architecture & layout

Presentation Outline

Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

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Conclusion

Questions & Comments

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- Successful concrete redesign
- Met all serviceability requirements
- Minimal impact interior architecture & layout

Façade Study Breadth:

- Matched existing thermal & moisture protection
- Cheaper
- Fast Construction

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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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Structural Depth;

- Successful concrete redesign
- Met all serviceability requirements
- Minimal impact interior architecture & layout

Façade Study Breadth:

- Matched existing thermal & moisture protection
- Cheaper
- Fast Construction

Schedule Impact Breadth:

- Develop an adjusted schedule
- Structure: + 3 months
- Façade: -6 months

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Building Introduction

Existing Structure

Problem Statement

Structural Depth

Façade Study Breadth

Schedule Impact Breadth

Conclusion

Questions & Comments

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Family & Friends

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Building Introduction

Existing Structure

Problem Statement

Structural Depth

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Questions & Comments

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Snow Load Type	Uniform (psf)
Flat Roof Load	21
Sloped Roof Load	24

Lvl 2	Area	DL	Weight
Slab	16600	46	763600
superimposed	16600	5	83000
Steel	16600	5	83000
Façade	8663	45	389812.5
CMU	8663	83	719029
Int Brick	2590	40	103600
Stone Floor	1700	10	17000
Total	16600		2,159,042
Lvl 3	Area	DL	Weight
Slab	16600	46	763600
superimposed	16600	5	83000
Steel	16600	5	83000
Façade	8820	45	396900
CMU	8820	83	732060
Int Brick	1400	40	56000
Stone Floor	1700	10	17000
			2,131,560
Lvl 4	Area	DL	Weight
Slab	16600	46	763600
superimposed	16600	5	83000
Steel	16600	5	83000
Façade	9293	45	418162.5
CMU	9293	83	771319
Int Brick	1500	40	60000
Stone Floor	1700	10	17000
			2,196,082
PH	Area	DL	Weight
Slab	6000	46	276000
Roof Deck	4700	3.3	15510
superimposed	10700	5	53500
Steel	10700	5	53500
Façade	9000	45	405000
CMU	9000	83	747000
Green Roof	4700	25	117500
			1,668,010
Roof	Area	DL	Weight
Slate	7310	10	73100
steel	7310	5	36550
superimposed	7310	5	36550
			146,200
Bld weight (lbs)			8,300,893

Appendix

Weight Comparison

Lvl 2	Area	DL	Weight
Slab	16600	63	1037500
superimposed	16600	5	83000
Steel	16600	0	0
Façade	8663	100	866250
Int Brick	2590	4.7	12086.667
Total	16600		2,032,837
Lvl 3	Area	DL	Weight
Slab	16600	63	1037500
superimposed	16600	5	83000
Steel	16600	0	0
Façade	8820	100	882000
CMU	8820	0	0
Int Brick	1400	4.7	6533.3333
Stone Floor	1700	20	34000
			2,043,033
Lvl 4	Area	DL	Weight
Slab	16600	63	1037500
superimposed	16600	5	83000
Steel	16600	0	0
Façade	9293	100	929250
CMU	9293	0	0
Int Brick	1500	4.7	7000
Stone Floor	1700	20	34000
			2,090,750
PH	Area	DL	Weight
Slab	6000	63	375000
Roof Deck	4700	63	293750
superimposed	10700	5	53500
Steel	10700	0	0
Façade	9000	100	900000
CMU	9000	0	0
Green Roof	4700	25	117500
			1,739,750
Roof	Area	DL	Weight
conc slab	7310	63	456875
Slate	7310	10	73100
steel	7310	0	0
superimposed	7310	5	36550
			566,525
Bld weight (lbs)			8,472,895

Appendix

Overturning Moment			
Level	ht (ft)	Wind Force (K)	Moment (k-ft)
Roof	67	40.83	2736
Parapet	63	15.68	988
PH	57	55.79	3180
4	42	74.23	3118
3	25	67.12	1678
2	14	61.48	861
Overturning Moment=			12,560 k-ft
Resisting Moment			
$M_{resist} = 8,473k \times 89' / 2 \times .67 = 252,622 \text{ k-ft}$			

PH Level				
N-S	ft	E-W	ft	ft
CR=	34	CR=	106	.15By= 36
CM=	32	CM=	115	.15Bx= 13
CR-CP=	2.00	CR-CP=	-9.00	

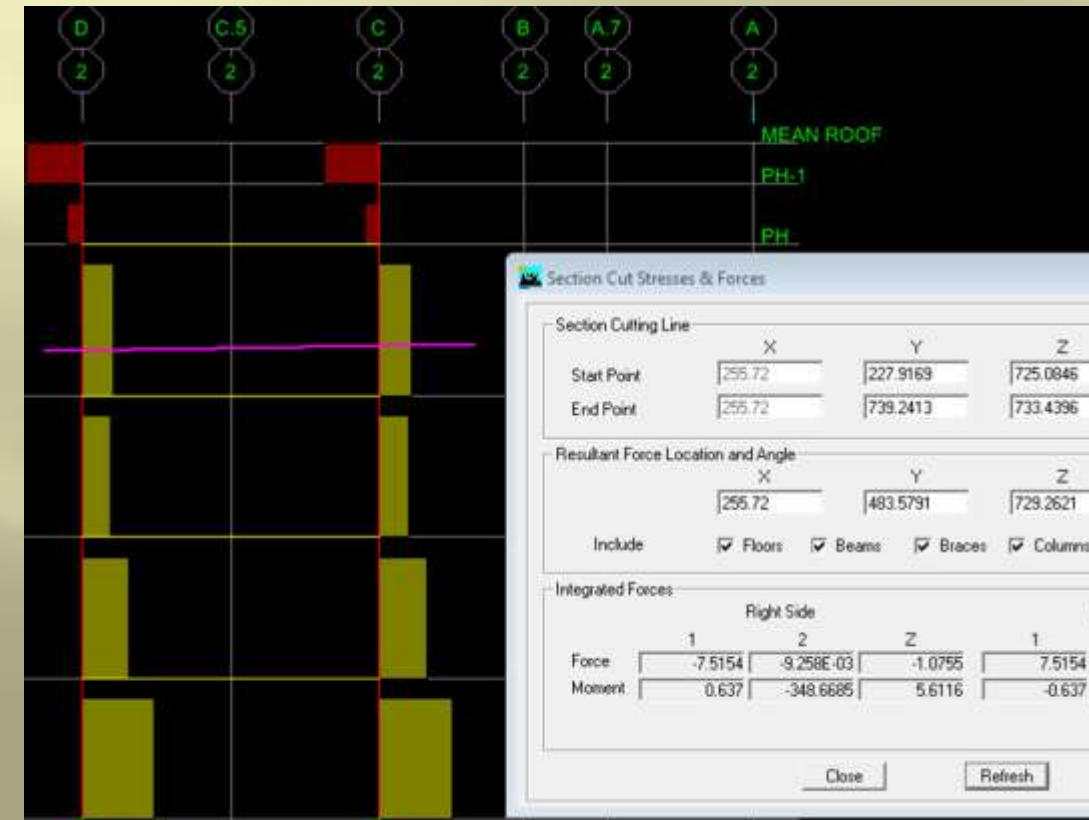
W1: Case 1 NS			
F_{NS} (kip)	112.3	e_{NS} (ft)	9
F_{EW} (kip)	0	e_{EW} (ft)	0
M_{NS} (k-ft)	1010.7		
M_{EW} (k-ft)	0		

Frame	K (k/in)	ΣK_{NS} (k/in)	ΣK_{EW} (k/in)	Direct shear (kip)	d (in)	Kd ²	ΣKd^2	Torsional Moment Shear (kip)	Total shear (kip)
B	0.5502	0.00	4.23	0.00	32.50	581.15	17444.38	1.04	1.04
C	1.2902	0.00	4.23	0.00	18.20	427.38	17444.38	1.36	1.36
D	1.3881	0.00	4.23	0.00	-11.30	177.25	17444.38	-0.91	-0.91
E	1.0000	0.00	4.23	0.00	-34.00	1156.00	17444.38	-1.97	-1.97
1	0.1972	3.51	0.00	6.32	-106.00	2215.32	17444.38	-1.21	5.10
2	0.2560	3.51	0.00	8.20	-84.70	1836.50	17444.38	-1.26	6.94
3	0.3437	3.51	0.00	11.01	-61.30	1291.35	17444.38	-1.22	9.79
4	0.4860	3.51	0.00	15.57	-30.70	458.02	17444.38	-0.86	14.70
5	0.5848	3.51	0.00	18.73	0.30	0.05	17444.38	0.01	18.74
6	0.5309	3.51	0.00	17.00	31.30	520.08	17444.38	0.96	17.97
7	0.4180	3.51	0.00	13.39	55.90	1306.04	17444.38	1.35	14.74
8	0.2922	3.51	0.00	9.36	85.00	2111.43	17444.38	1.44	10.80
9	0.2248	3.51	0.00	7.20	106.00	2525.70	17444.38	1.38	8.58
10	0.1727	3.51	0.00	5.53	128.20	2838.10	17444.38	1.28	6.81

Case 2 NS + .15By

$.75F_{NS}$ (kip)	84.225	e_{NS} (ft)	45
$.75F_{EW}$ (kip)	0	e_{EW} (ft)	0
M_{NS} (k-ft)	3790.125		
M_{EW} (k-ft)	0		

Frame	K (k/in)	ΣK_{NS} (k/in)	ΣK_{EW} (k/in)	Direct shear (kip)	d (ft)	Kd ²	ΣKd^2	Torsional Moment Shear (kip)	Total shear (kip)
B	0.5502	0.00	4.23	0.00	32.50	581.15	17444.38	3.89	3.89
C	1.2902	0.00	4.23	0.00	18.20	427.38	17444.38	5.10	5.10
D	1.3881	0.00	4.23	0.00	-11.30	177.25	17444.38	-3.41	-3.41
E	1.0000	0.00	4.23	0.00	-34.00	1156.00	17444.38	-7.39	-7.39
1	0.1972	3.51	0.00	4.74	-106.00	2215.32	17444.38	-4.54	0.20
2	0.2560	3.51	0.00	6.15	-84.70	1836.50	17444.38	-4.71	1.44
3	0.3437	3.51	0.00	8.26	-61.30	1291.35	17444.38	-4.58	3.68
4	0.4860	3.51	0.00	11.67	-30.70	458.02	17444.38	-3.24	8.43
5	0.5848	3.51	0.00	14.05	0.30	0.05	17444.38	0.04	14.09
6	0.5309	3.51	0.00	12.75	31.30	520.08	17444.38	3.61	16.36
7	0.4180	3.51	0.00	10.04	55.90	1306.04	17444.38	5.08	15.12
8	0.2922	3.51	0.00	7.02	85.00	2111.43	17444.38	5.40	12.42
9	0.2248	3.51	0.00	5.40	106.00	2525.70	17444.38	5.18	10.58
10	0.1727	3.51	0.00	4.15	128.20	2838.10	17444.38	4.81	8.96



Appendix

Column Design

Check for LL Reduction at 2 ext. & 2 int. col

$$L = L_o \left(0.25 + \frac{15}{\sqrt{K_{12} A_1}} \right)$$

Ext Col E5

$$LL = 100 \left(0.25 + \frac{15}{\sqrt{4(311 \frac{2400}{2})}} \right) = 65 \text{ psf}$$

Int Col D.5

$$LL = 100 \left(0.25 + \frac{15}{\sqrt{4(51 \times 24)}} \right) = 52 \text{ psf}$$

Slab DL

$$DL_{\text{slab}} = 150 \text{ yd}^3 \times \frac{5}{27} = 62.5 \text{ psf}$$

Design Combs:

$$1.2D + 1.0L + 1.6W$$

$$\sum P_u = 14528$$

$$U_s = 322 \text{ K}$$

$$A_c = 0.0021$$

$$Q = \frac{\sum P_u \Delta_c}{U_s l_c} = \frac{(14528)(0.0021)}{(322)(148)} = 5.37 \times 10^{-4} < 0.05 \therefore \text{Non-Sway Frame}$$

Ext Col C-9 L3

Elabs Info:

- Design Combs - 7. : 1.2D + 1.0L + 1.6W
- $P_u = 530 \text{ K}$
- $M_u = 280 \text{ F-T}$

Use Appendix A Form w/19 5th ed.

$$h = 20'$$

$$\gamma = 0.75$$

$$c = \frac{280(12)}{530} = 6.3$$

$$\frac{c}{h} = \frac{6.3}{20} = 0.32$$

$$\frac{\phi P_u}{bh} = \frac{530}{(18)(20)} = 1.47$$

$$\frac{\phi M_u}{bh^2} = \frac{280(12)}{18(20)^2} = 0.47$$

- $f_c = 4000, f_y = 60$
- $\gamma = 0.75$
- $\beta = 0.023$
- $\beta = 0.023 = 2.3\% < 0.8\% \checkmark$
- $A_{s \text{ req}} = (0.023)(18)(20) = 8.3 \text{ in}^2$ use **12#9 $A_s = 12.00 \text{ in}^2$**

Per floor					
Column Reinforcement	6.80	6.8 TONS	2.3	3.0	Starts 7 days after beam and slab pour
Column Forming	1235	1235 SF	238	5.2	Starts 1 day after Column Reinf
Pour Columns	37	37 CY	92	0.4	
Beam Forming	6200	6200 SF	650	9.5	use 2 crews Beam and Slab form starts 2 days after column form
Beam Reinf	10.1	10.1 TONS	2.7	3.7	beam reif starts 4 days before beam and slab form ends
Slab Forming	5500	5500 SF	1100	5.0	use 2 crews
Slab Reinf	4.1	4.1 TONS	2.9	1.4	
Pour Slab and Beams	210	210 CY	120	1.8	
Precast Panels	4107	4107 SF	3000	15 total per sequence	

28. How many panels can be installed in a day?
 Depending on site access and the orientation of panels on a building, between 3,000 to 4,500 square feet of wall area can be installed each day.

